

Accelerated landings in stingless bees are triggered by visual threshold cues

Supplementary Material

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Text S1: Calculation of the angular size and rate of expansion of the target during landing:

Consider a landing *Scaptotrigona depilis* with the spatial coordinates x-y-z flying at a linear speed V and at a distance D from the centre of the artificial target of diameter S. We wish to determine the angular size of the target θ^T and the angular rate of expansion $d\theta^T/dt$.

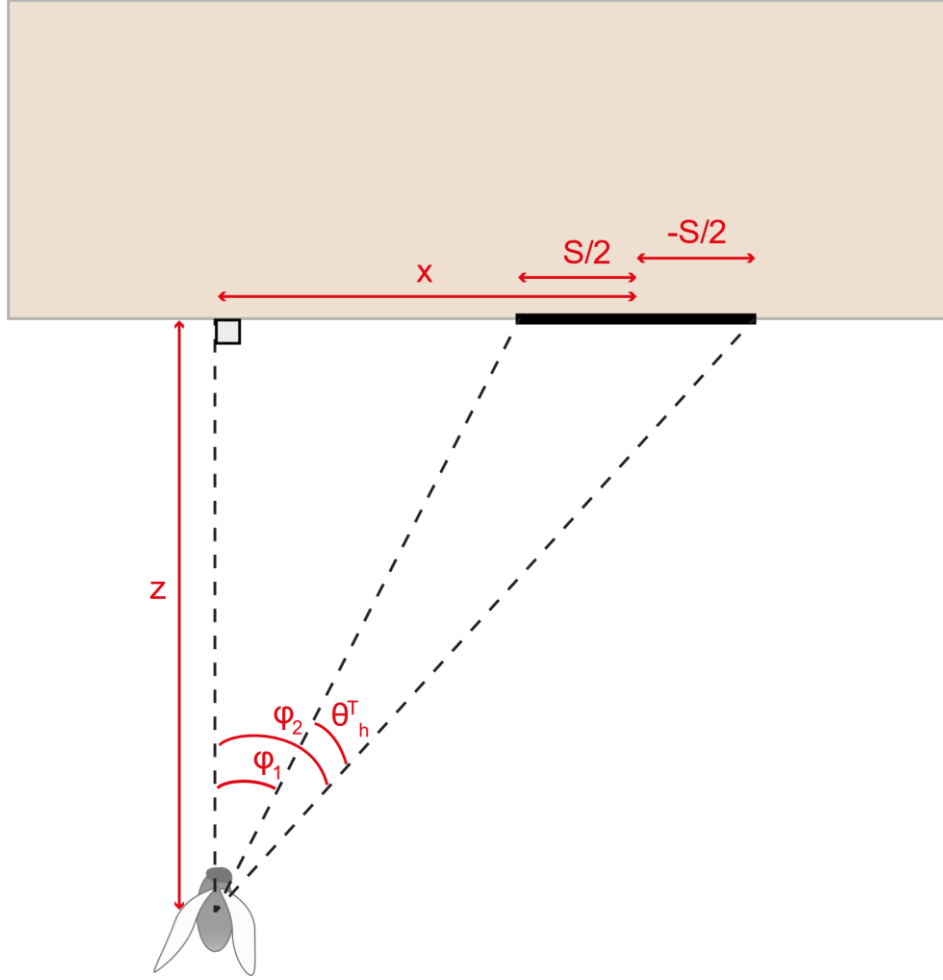


Figure S1: Framework for the calculation of the horizontal component of the angular size of the target θ_h^T . The landing bee has the spatial coordinates x-y-z and the linear speed V. The beige rectangle represents the hive box. The black bar is the target of diameter S.

1) Calculation of the angular size θ^T

Given θ_h^T the horizontal component of θ^T . As schematised in Figure S1:

$$\theta_h^T = \varphi_2 - \varphi_1$$

Therefore, by using the inverse tangent function - Arctan:

$$\theta_h^T = \text{Arctan}\left(\frac{x + \frac{S}{2}}{z}\right) - \text{Arctan}\left(\frac{x - \frac{S}{2}}{z}\right)$$

As θ_h^T is in the range $[-90, 90]$ deg, we can use the formula $\text{Arctan}(a) - \text{Arctan}(b) = \text{Arctan}\left(\frac{a-b}{1+ab}\right)$:

$$\theta^T_h = \text{Arctan} \left(\frac{\frac{x + \frac{S}{2}}{z} - \frac{x - \frac{S}{2}}{z}}{1 + \left(\frac{x + \frac{S}{2}}{z} \right) \left(\frac{x - \frac{S}{2}}{z} \right)} \right)$$

Therefore:

$$\theta^T_h = \text{Arctan} \left(\frac{\frac{S}{z}}{1 + \frac{x^2 - \frac{S^2}{4}}{z^2}} \right)$$

Hence:

$$\theta^T_h = \text{Arctan} \left(\frac{Sz}{z^2 + x^2 - \frac{S^2}{4}} \right)$$

Given θ^T_v the vertical component of θ^T , θ^T is the average of its vertical and horizontal components:

$$\theta^T = \frac{\theta^T_h + \theta^T_v}{2}$$

Hence equation 1:

$$\text{Eq1: } \theta^T = \frac{1}{2} \text{Arctan} \left(\frac{Sz}{z^2 + x^2 - \frac{S^2}{4}} \right) + \frac{1}{2} \text{Arctan} \left(\frac{Sz}{z^2 + y^2 - \frac{S^2}{4}} \right)$$

2) Calculation of the absolute and relative angular speed

We take equation 2 from Baird et al 2015:

$$\text{Eq 2: } \frac{d\theta^T}{dt} \approx \frac{V \sin 2\theta^T}{2D}$$

Where $d\theta^T/dt$ is the rate of expansion of the target. And the rate of expansion relative to θ^T is:

$$\frac{d\theta^T}{\theta^T dt}$$

Text S2: Calculation of predicted values of angular size at landing initiation (LI) and leg extension (LE) in four landing control hypotheses:

(1) *Constant angular size hypothesis*

at LI and LE, for every bee:

$$\theta^T_{(1)} = \overline{\theta^T}$$

Where $\overline{\theta^T}$ is the average value of angular size over all the bees.

(2) *Constant distance to the target hypothesis*

at LI and LE, per definition:

$$D^2 = x^2 + y^2 + z^2$$

With Eq1, for every bee:

$$\theta^T_{(2)} = \frac{1}{2} \text{Arctan} \left(\frac{Sz}{\overline{D}^2 + y^2 - \frac{S^2}{4}} \right) + \frac{1}{2} \text{Arctan} \left(\frac{Sz}{\overline{D}^2 + x^2 - \frac{S^2}{4}} \right)$$

Where $\overline{D}$ is the value of the distance to the target averaged across all flights.

(3) *Constant absolute rate of expansion hypothesis*

With Eq2, for every bee at LI and LE:

$$\overline{\left(\frac{d\theta^T}{dt} \right)} = \frac{V \sin 2\theta^T_{(3)}}{D}$$

$$\theta^T_{(3)} = \frac{1}{2} \text{Arcsin} \left(\frac{\overline{\left(\frac{d\theta^T}{dt} \right)} D}{V} \right)$$

Where $\overline{\left(\frac{d\theta^T}{dt} \right)}$ is the value of the rate of expansion averaged across all flights.

(4) *Constant relative rate of expansion hypothesis*

at LI and LE for every bee:

$$\theta^T_{(4)} \overline{\left(\frac{d\theta^T}{\theta^T dt} \right)} = \frac{V \sin 2\theta^T_{(4)}}{D}$$

Where $\overline{\left(\frac{d\theta^T}{\theta^T dt} \right)}$ is the value of the rate of expansion relative to θ^T averaged across all flights.

By isolating $\theta^T_{(4)}$:

$$\text{Eq3: } \frac{\sin 2\theta^T_{(4)}}{2\theta^T_{(4)}} = \frac{D \overline{\left(\frac{d\theta^T}{\theta^T dt} \right)}}{V}$$

Given the Taylor series, for every real number x:

$$\sin x = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \frac{x^7}{7!} + \dots$$

Hence

$$\frac{\sin x}{x} = 1 - \frac{x^2}{3!} + \frac{x^4}{5!} - \frac{x^6}{7!} + \dots$$

To solve equation 3, we look for solutions to the equation:

$$1 - \frac{D\left(\frac{d\theta^T}{\theta^T dt}\right)}{V} + \frac{x^2}{3!} + \frac{x^4}{5!} + \frac{x^6}{7!} + \dots = 0$$

Given $X = x^2$:

$$1 - \frac{D\left(\frac{d\theta^T}{\theta^T dt}\right)}{V} + \frac{X}{3!} + \frac{X^2}{5!} \approx 0$$

Given X_1 is the positive solution to this second-degree equation, then the solution to equation 3 is:

$$\theta^T_{(4)} = \frac{\sqrt{X_1}}{2}$$

Reference:

Baird E, Boeddeker N, Ibbotson MR, Srinivasan M V. 2013 A universal strategy for visually guided landing. Pnas 110, 18686–18691.
doi:10.1073/pnas.1314311110/-/DCSupplemental. www.pnas.org/cgi/doi/10.1073/pnas.1314311110

Supplementary movies:

Merged recordings from the two synchronised cameras of landings separated by condition (C_{position} and C_{size}) and hive. The recordings were compressed and slowed down 4.8 times to reduce file size (original frame rate = 120 frames.s⁻¹). The recordings for C_{control} are available as supplementary material in Tichit et al. 2020.

formula	Sampling distribution (family)	Expected values (mu)	Variance (V)	Random effect of the hive (V)	Degree of belief (nu)	Residual variance (V)	Degree of belief (nu)	Number of iterations	burnin	thin
1 + S	Gaussian	0 0	10^8 0 0 10^8	1	50	1	0.0002	1 100 000	100 000	100

Table S1:

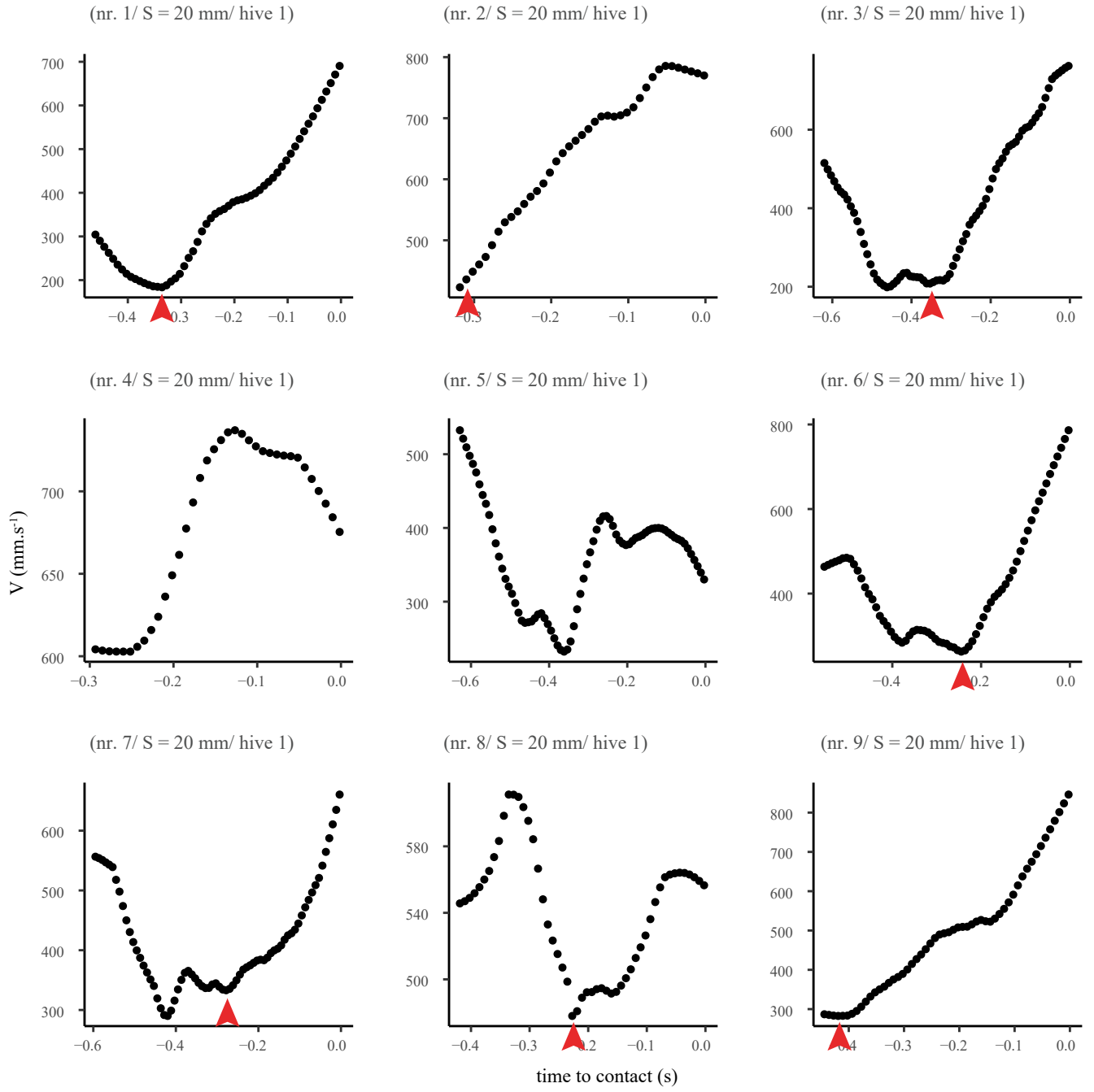
Parameters of the linear mixed models using Markov Chain Monte Carlo techniques of landing variables with target size (S) as a fixed effect and hive as a random variable. Details on each parameter are provided in the documentation of the MCMCglmm package in R.

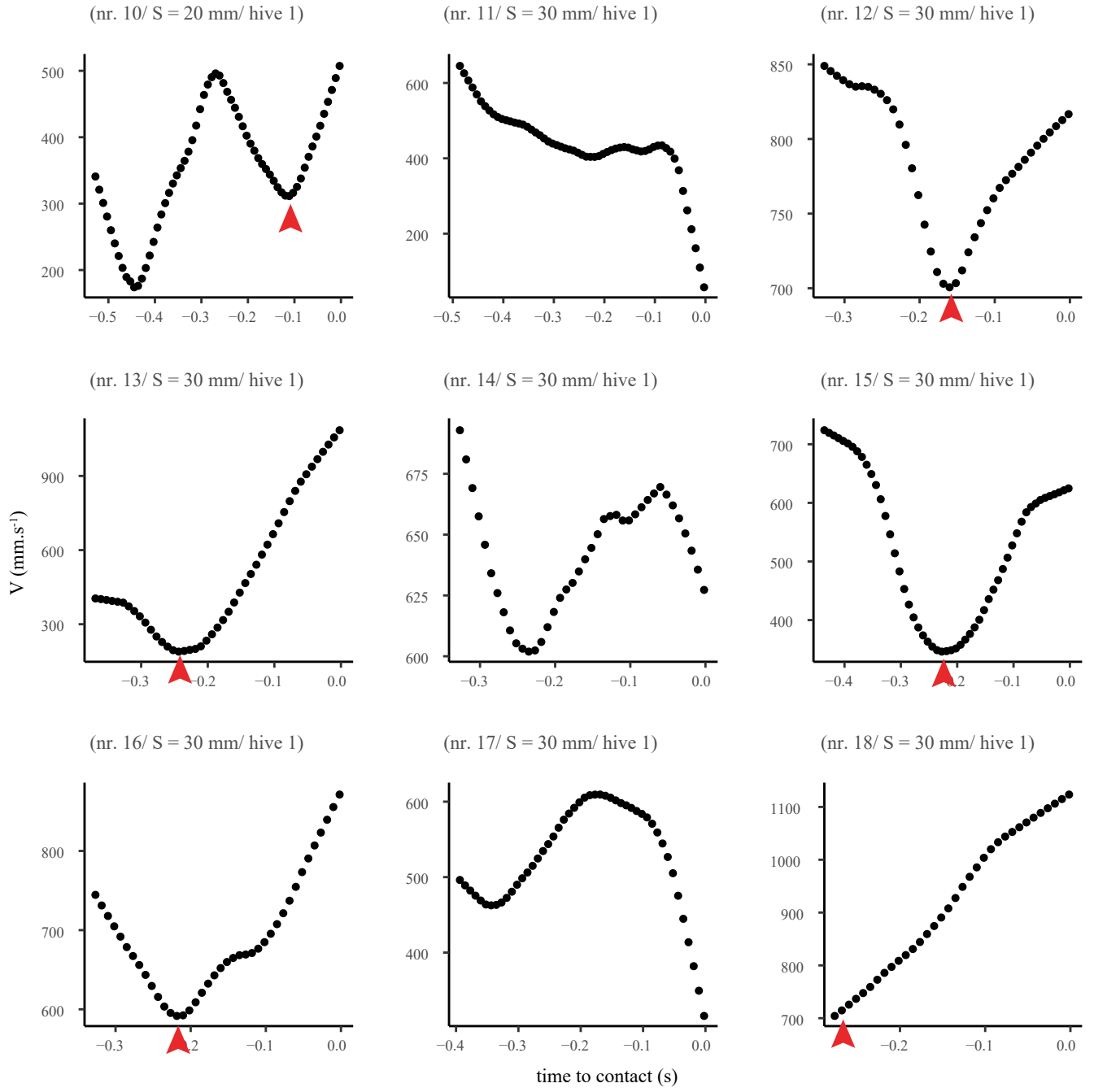
parameter	unit	formula	Deviance Information Criterion	Intercept	p_{MCMC}	CI	slope	p_{MCMC}	CI
$\theta_{\text{LI}}^{\text{r}}$	deg	1 + S	194	5.3	ns	[-0.88; 12]	0.26	**	[0.079; 0.45]
α	mm.s ⁻²	1 + S	495	1425	**	[357; 2372]	0.45	ns	[-27; 30]
$\theta_{\text{LE}}^{\text{r}}$	deg	1 + S	237	41	**	[17; 64]	0.13	ns	[-0.52; 0.78]
x_{end}	mm	1 + S	224	1.4	ns	[-9.3; 12]	-0.016	ns	[-0.33; 0.29]
y_{end}	mm	1 + S	204	3.0	ns	[-4.5; 11]	0.25	*	[0.017; 0.47]

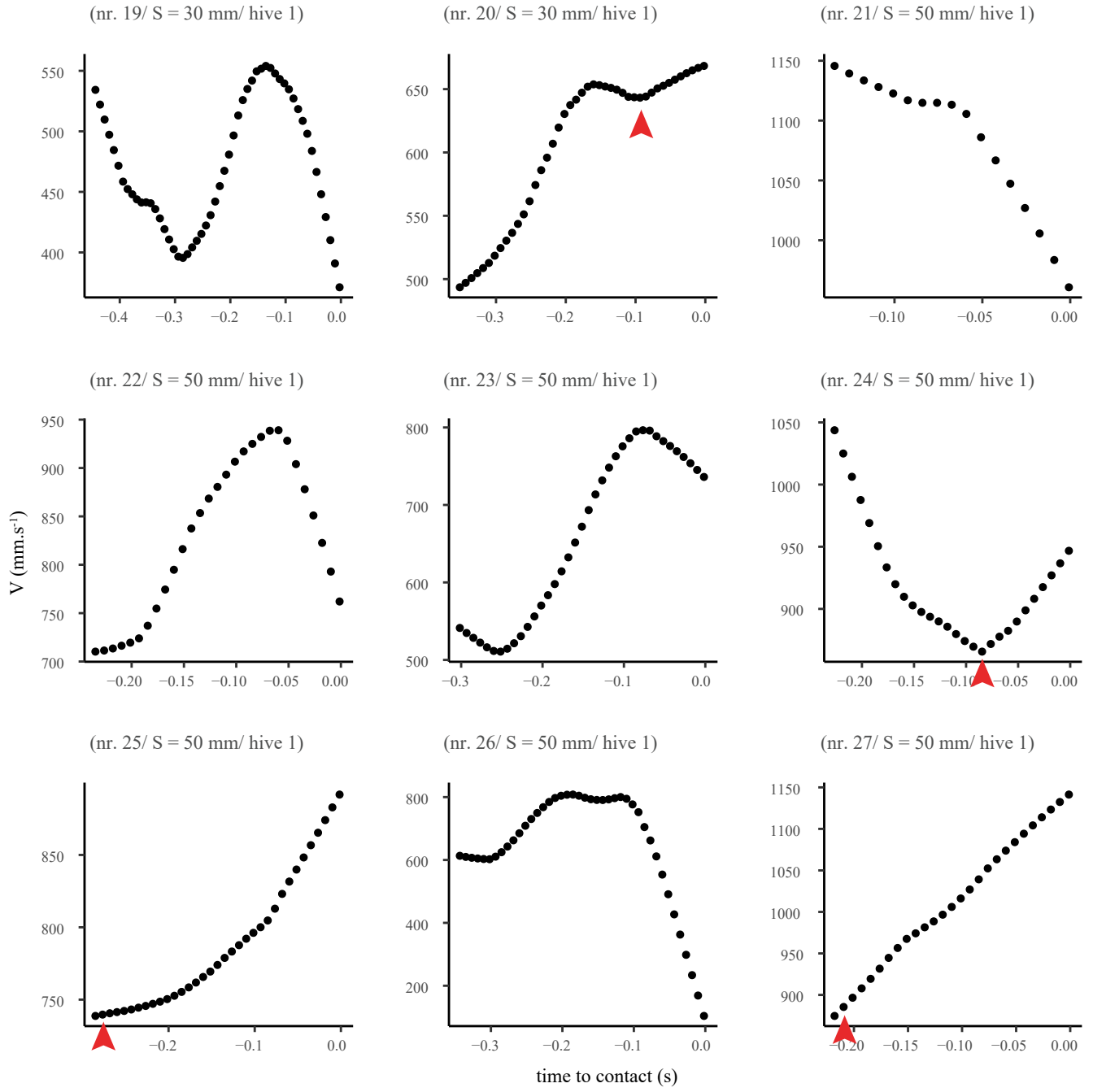
parameter	unit	formula	Deviance Information Criterion	Intercept	p_{MCMC}	CI	slope	p_{MCMC}	CI
$\theta_{\text{LI}}^{\text{r}}$	deg	1 + S	271	9.6	*	[1.1; 18]	0.097	ns	[-0.13; 0.32]
α	mm.s ⁻²	1 + S	605	1033	**	[294; 1712]	13	ns	[-5.1; 32]
$\theta_{\text{LE}}^{\text{r}}$	deg	1 + S	150	31	ns	[-16; 76]	0.35	ns	[-0.64; 1.4]
x_{end}	mm	1 + S	284	-10		[-21; 1.3]	0.31	*	[-0.0041; 0.61]
y_{end}	mm	1 + S	218	-2.6	ns	[-7.2; 2.0]	0.34	***	[0.23; 0.47]

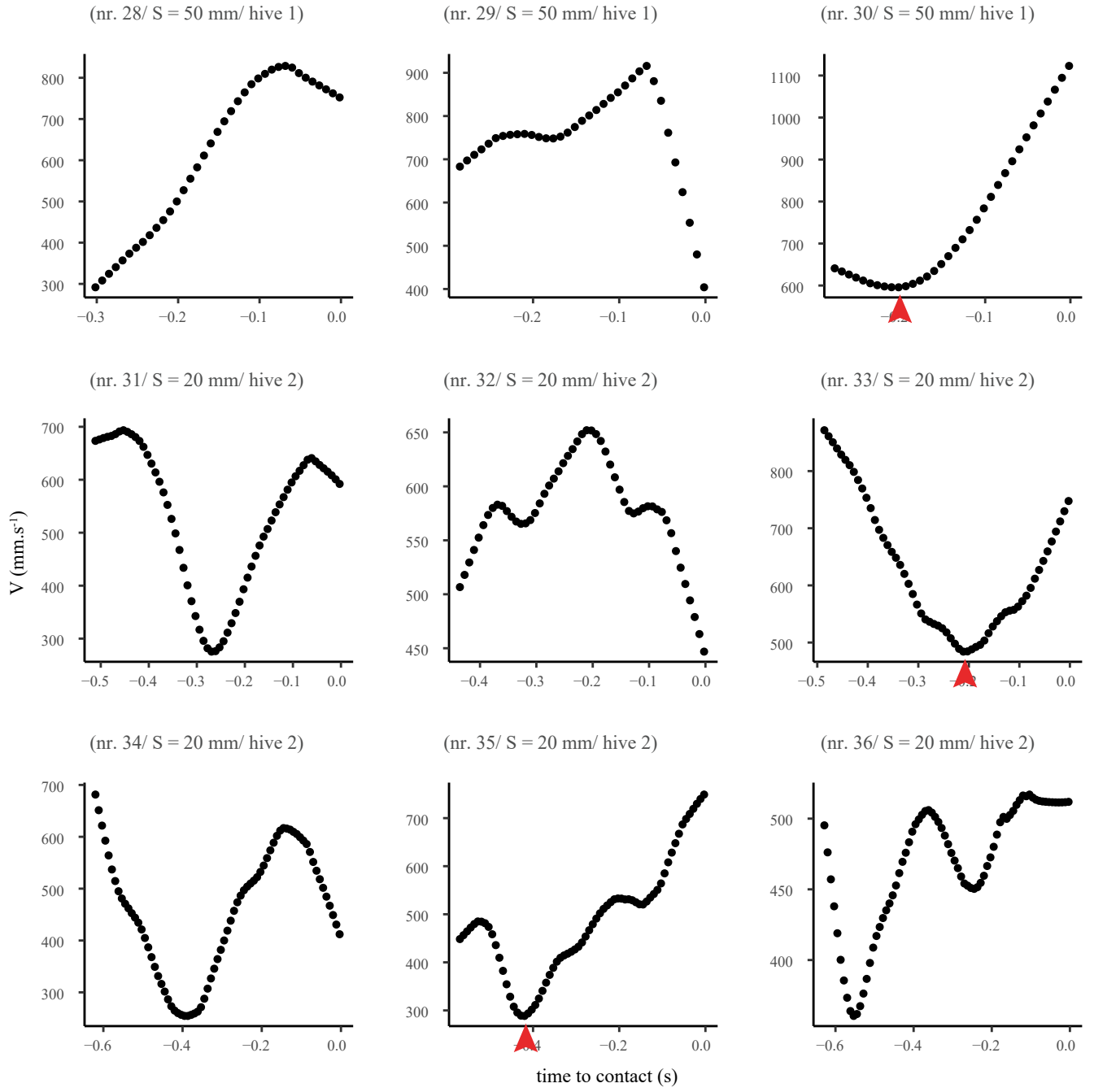
Table S2:

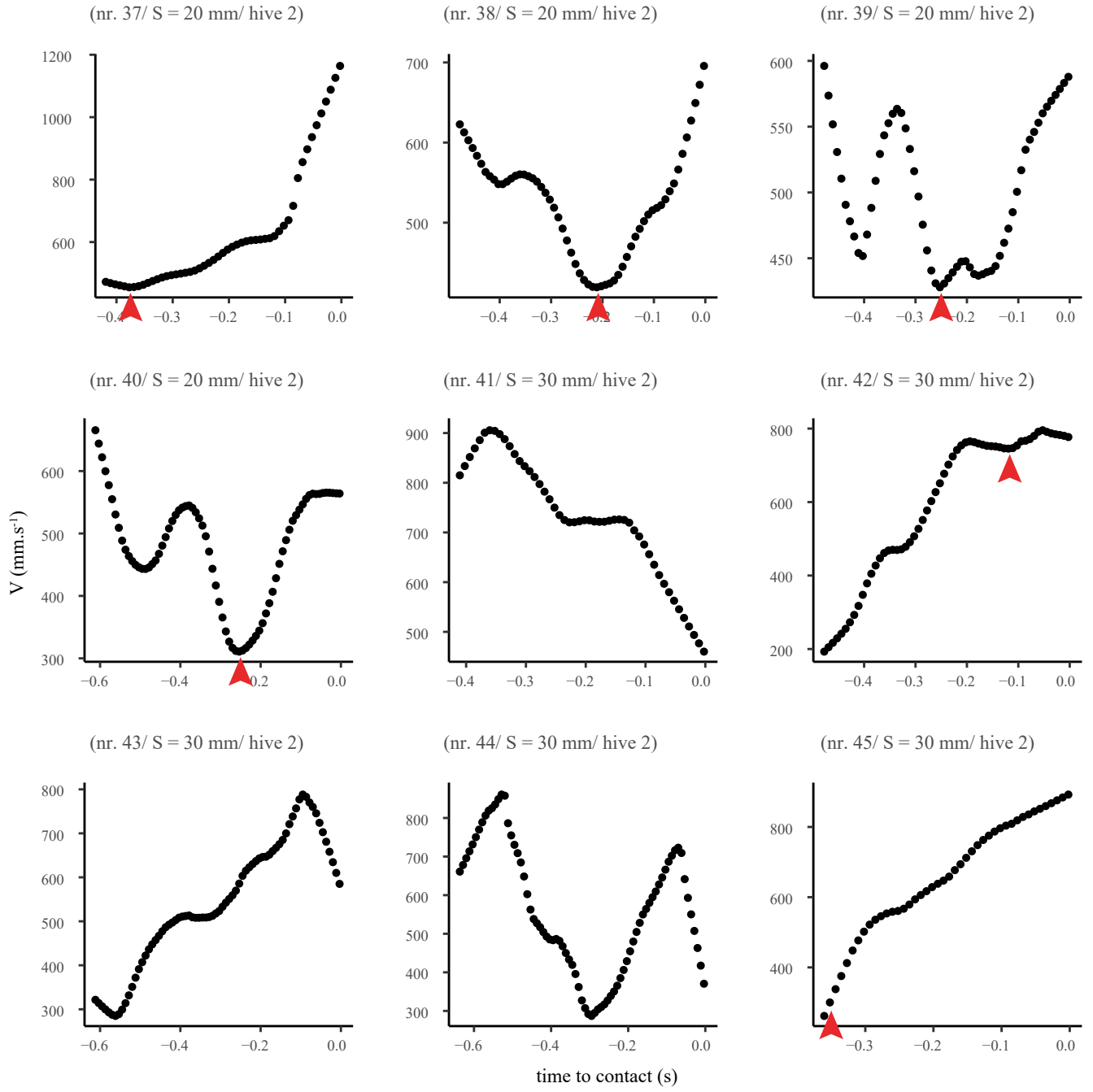
Linear mixed models of landing parameters in C_{size} with MCMC when separated between hive 1 (upper table) and hive 2 (lower table). The significances of the intercepts and slopes are given by the 95% credible interval (CI) and the bayesian p-value (p_{MCMC}). Significance codes: $<10^{-3}$ ***; $<10^{-2}$ **; <0.05 *; >0.05 ns.

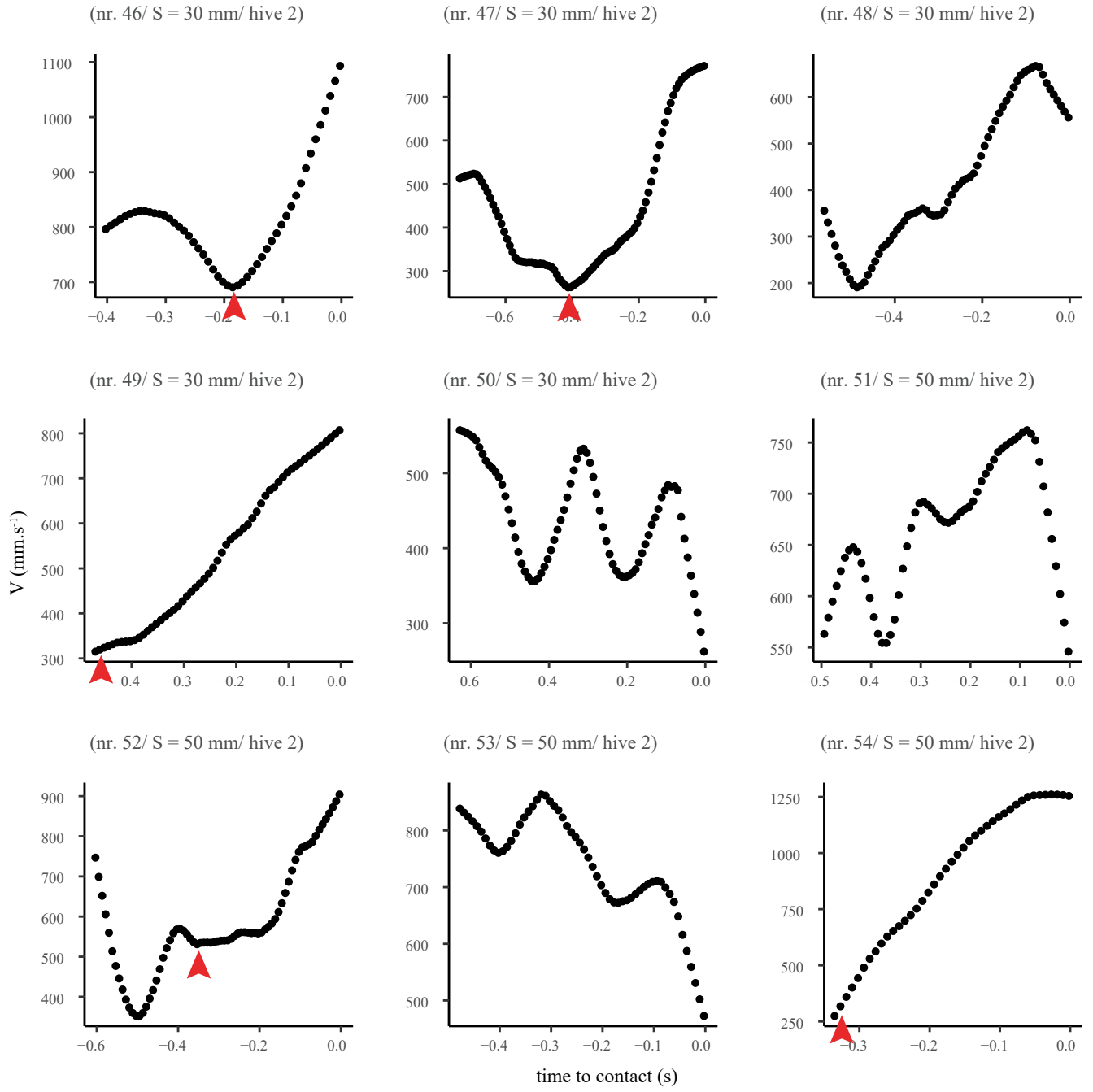


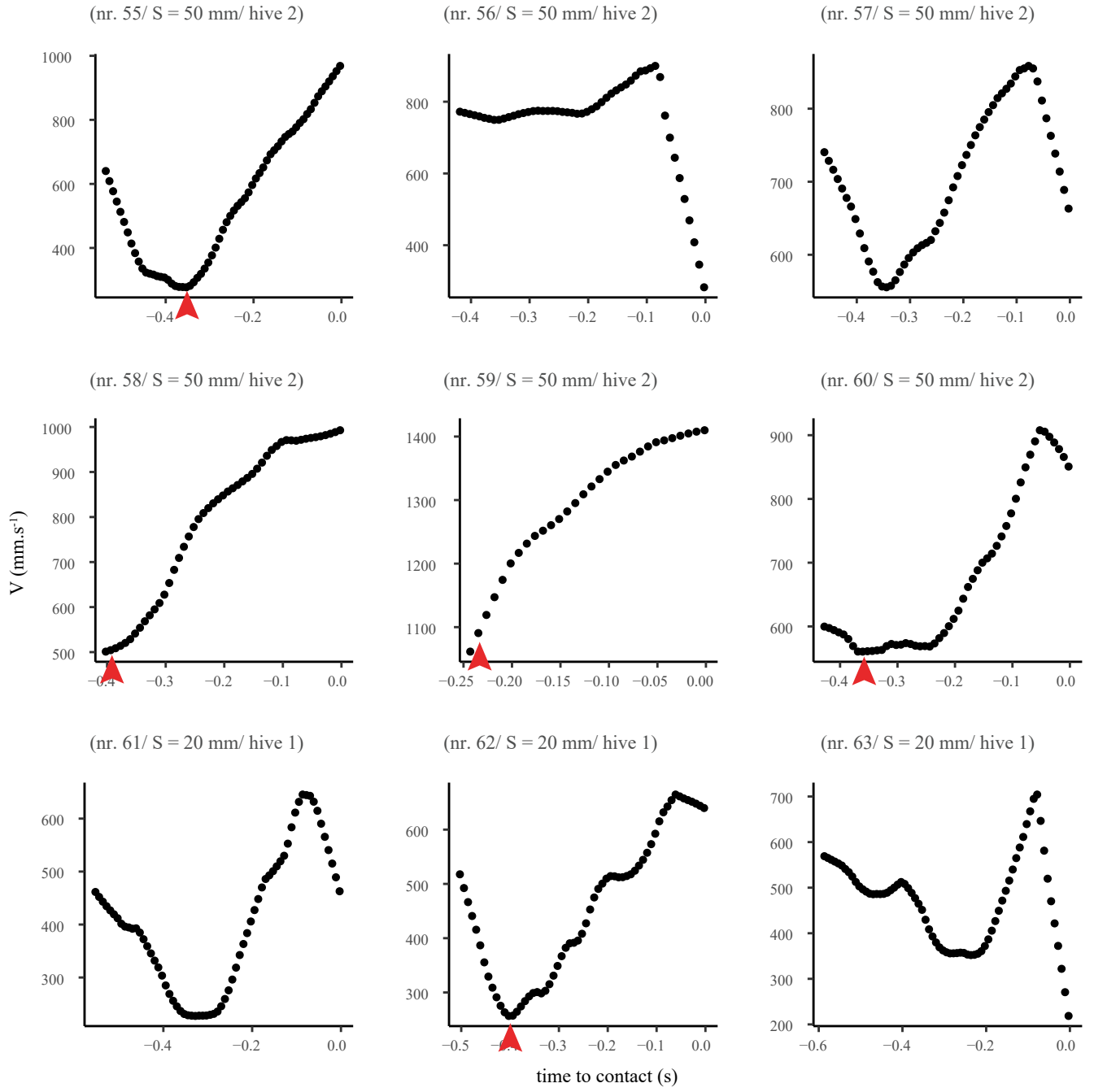


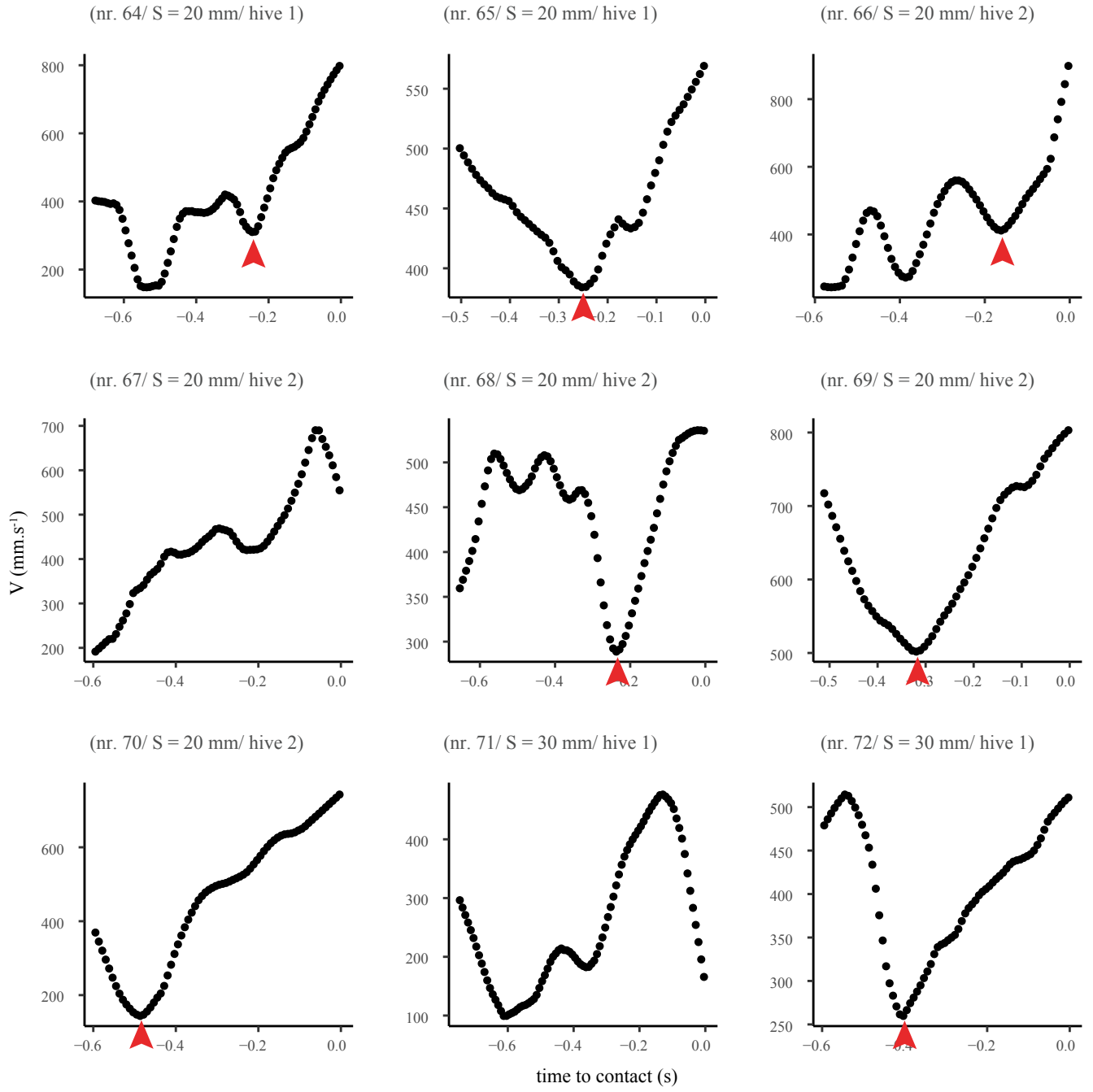




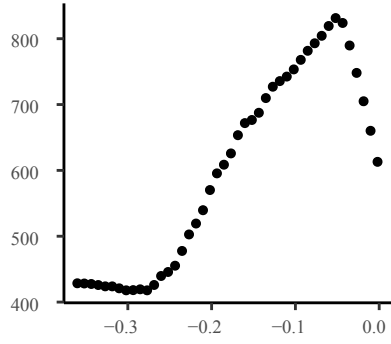




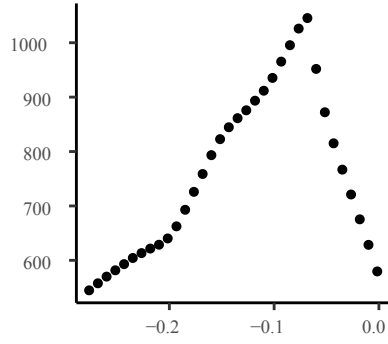




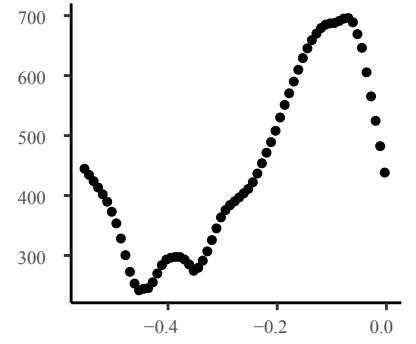
(nr. 73/ S = 30 mm/ hive 1)



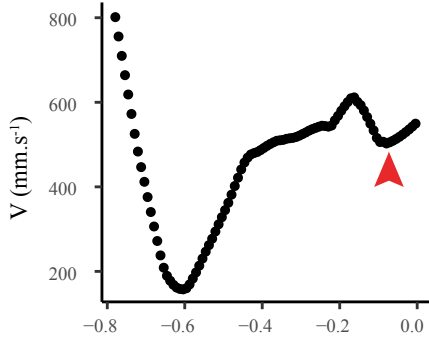
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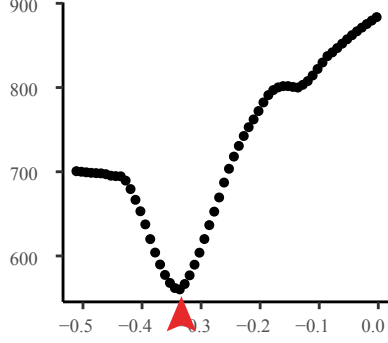
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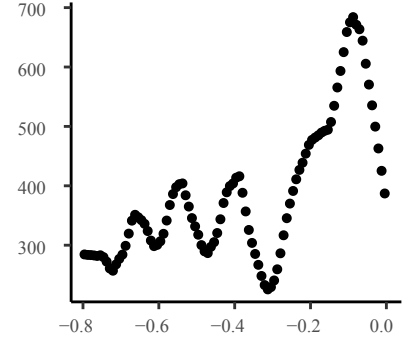
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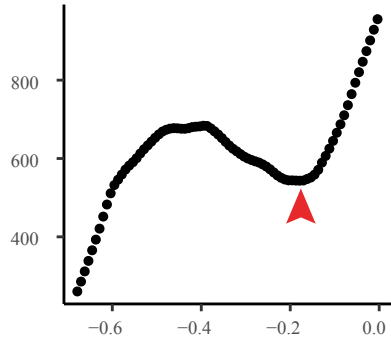
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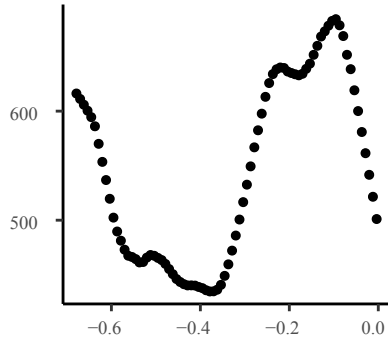
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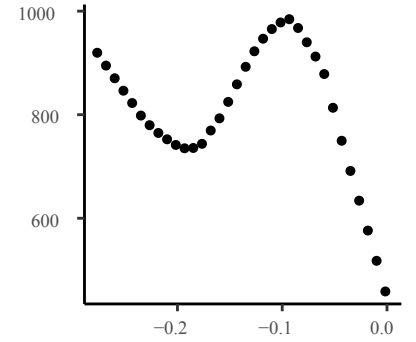
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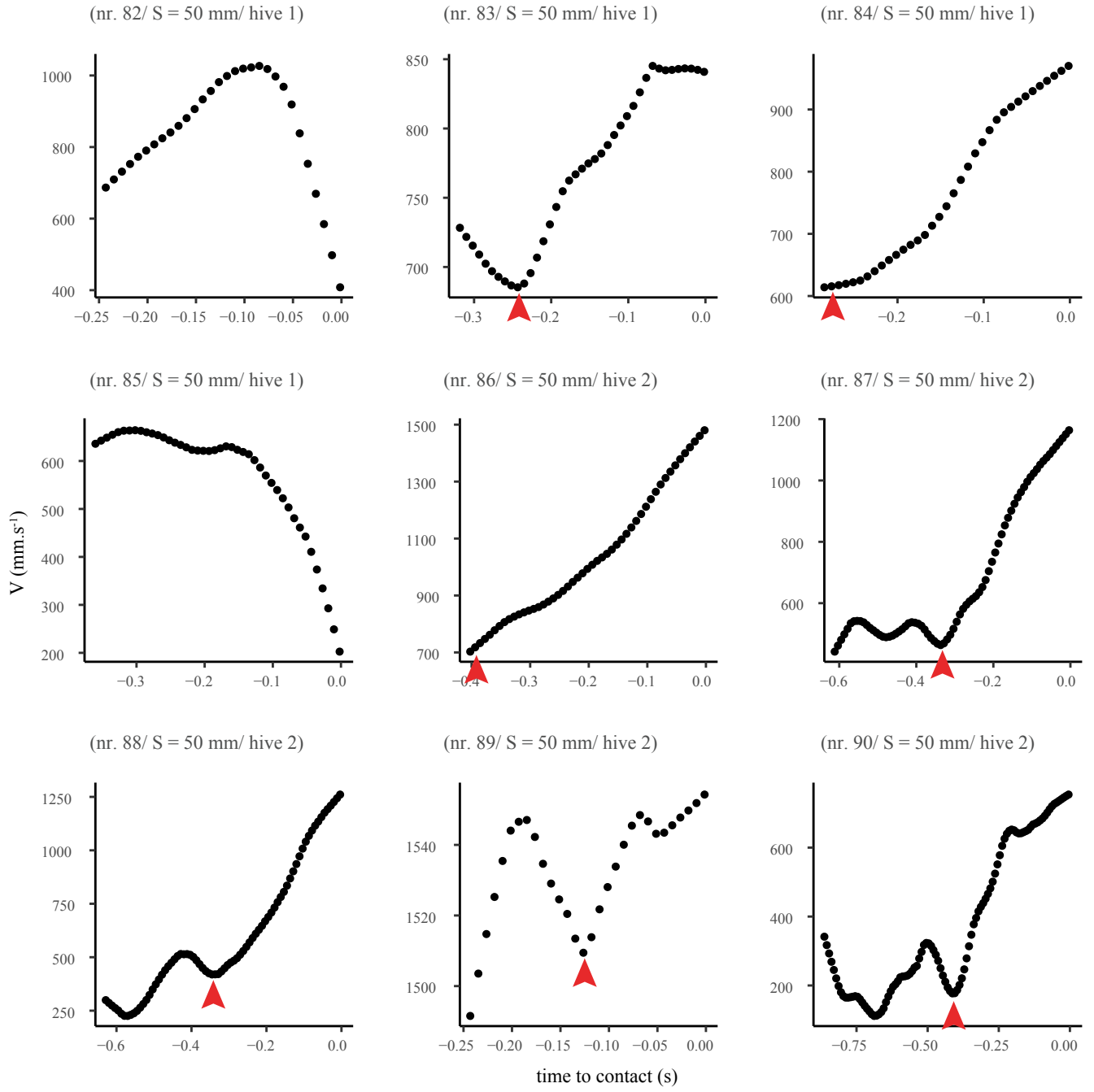
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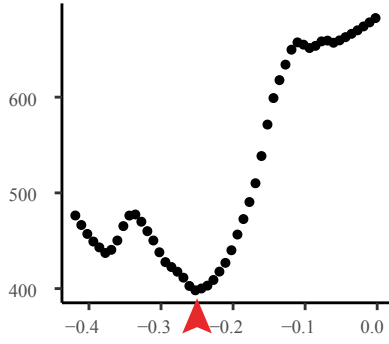
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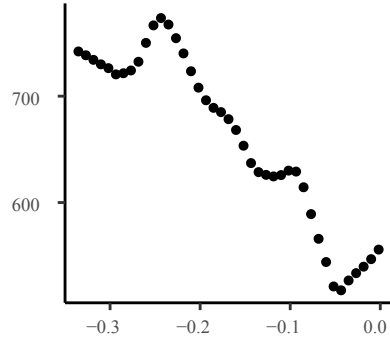
time to contact (s)



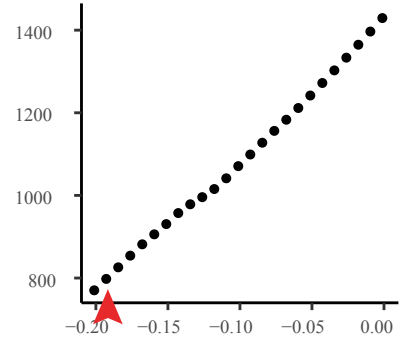
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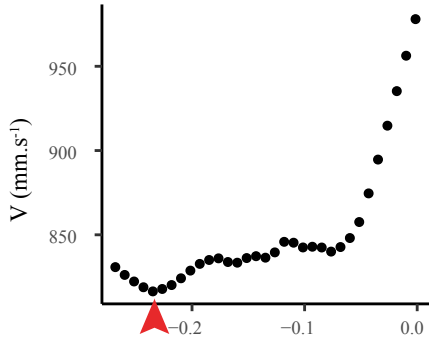
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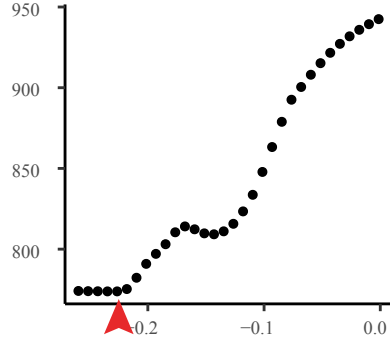
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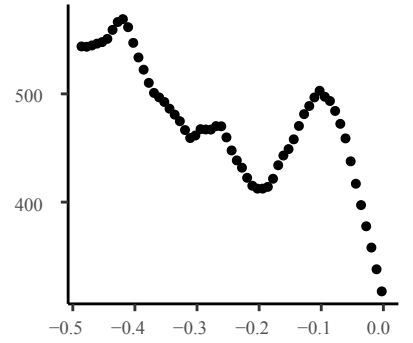
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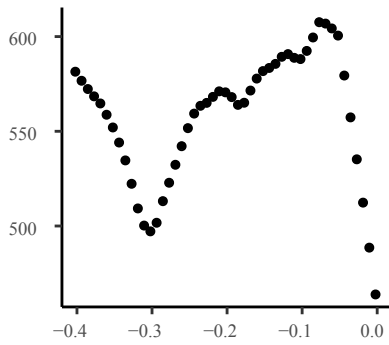
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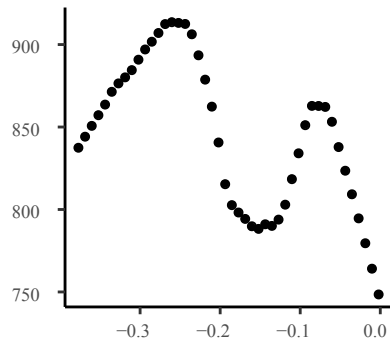
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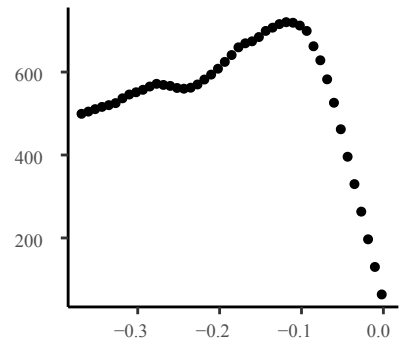
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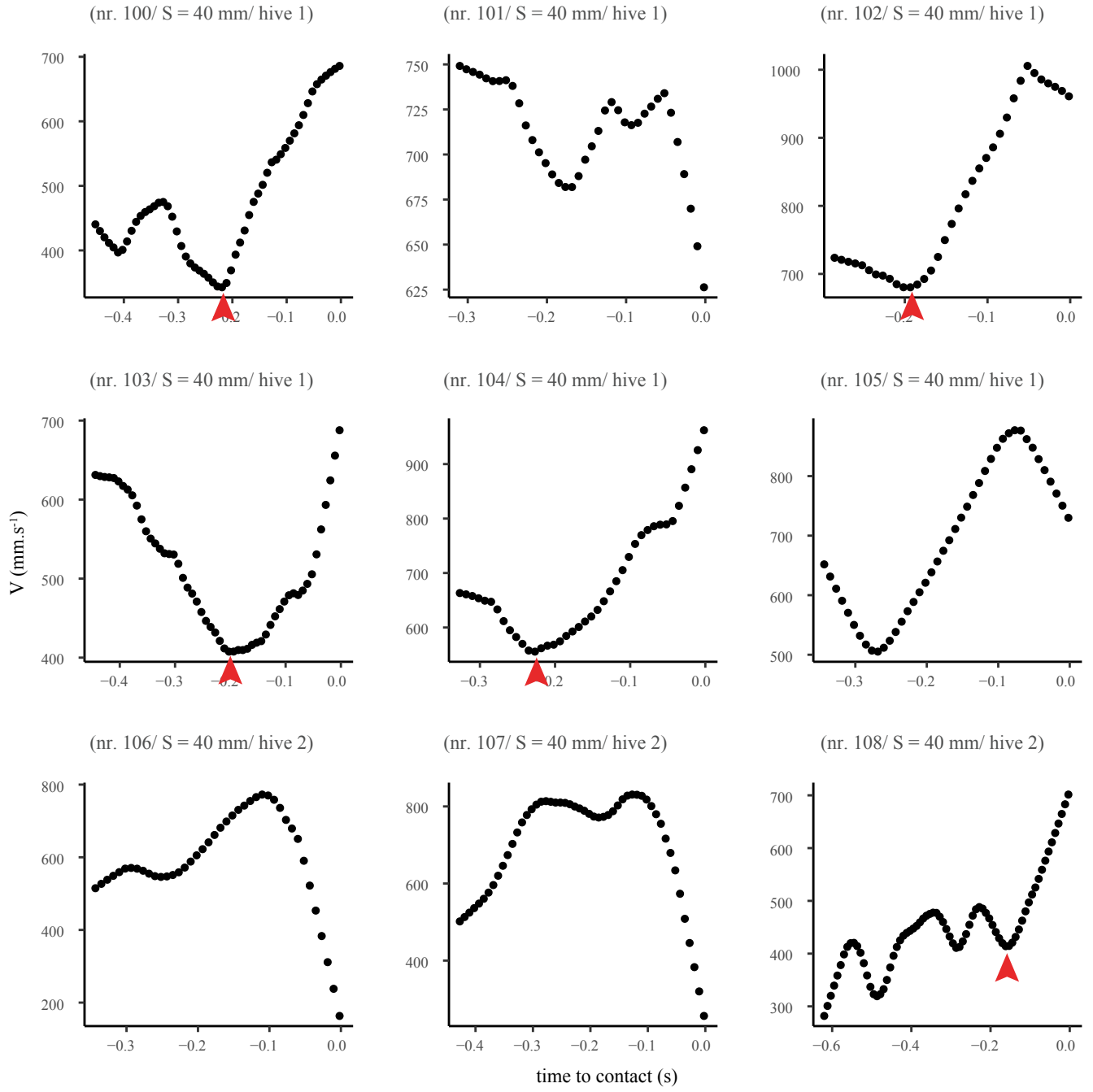
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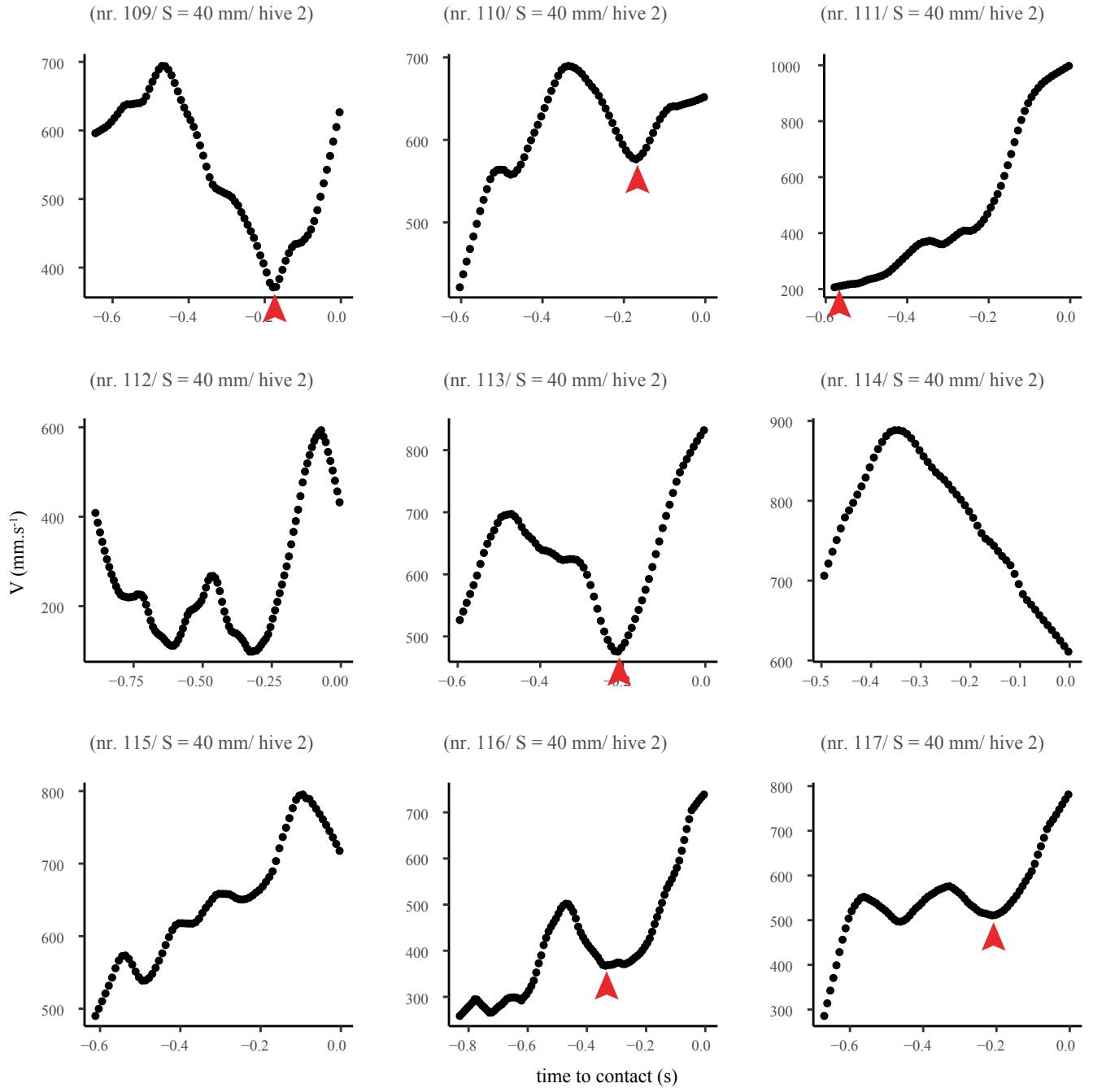


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time to contact (s)





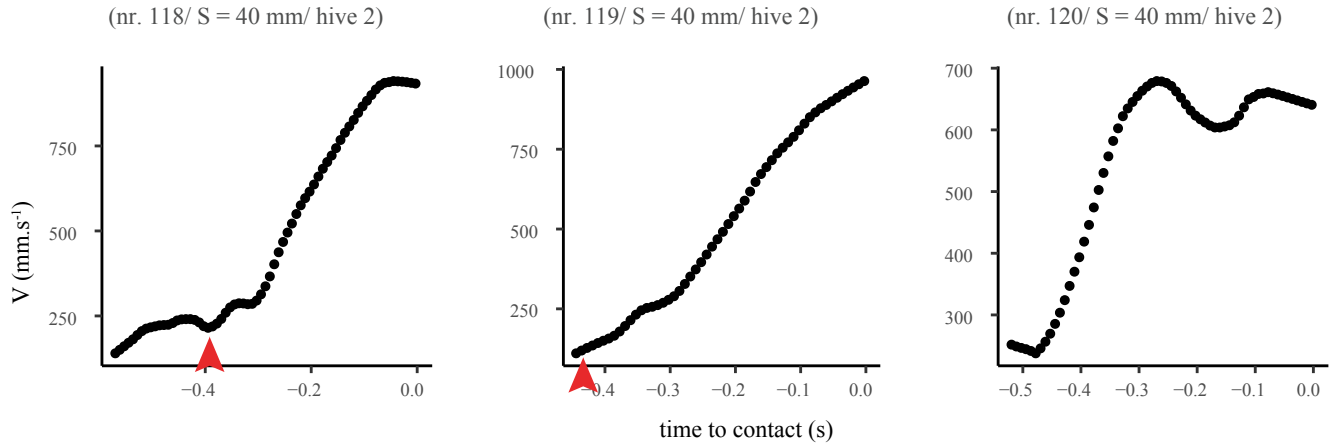
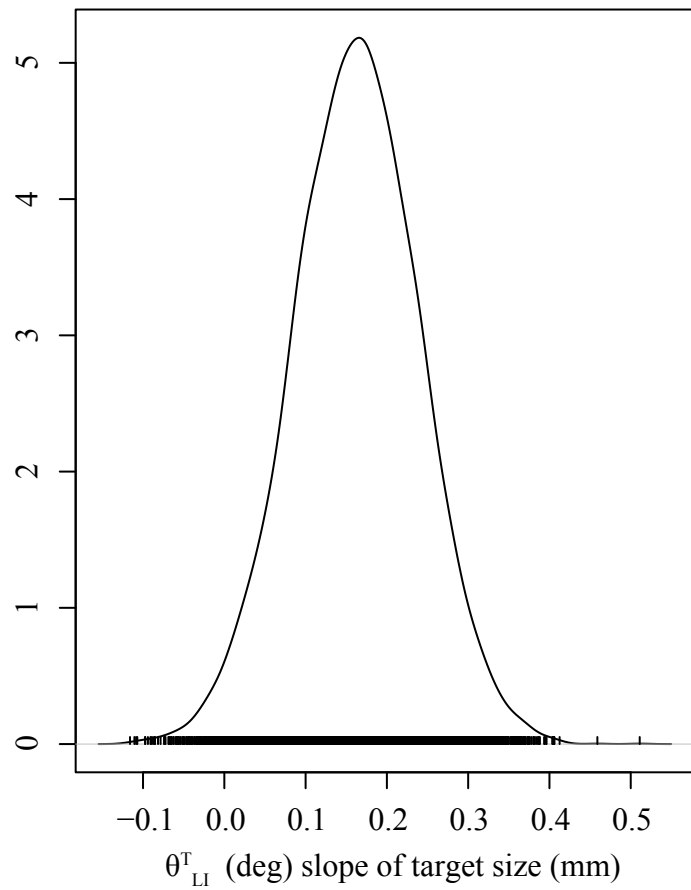
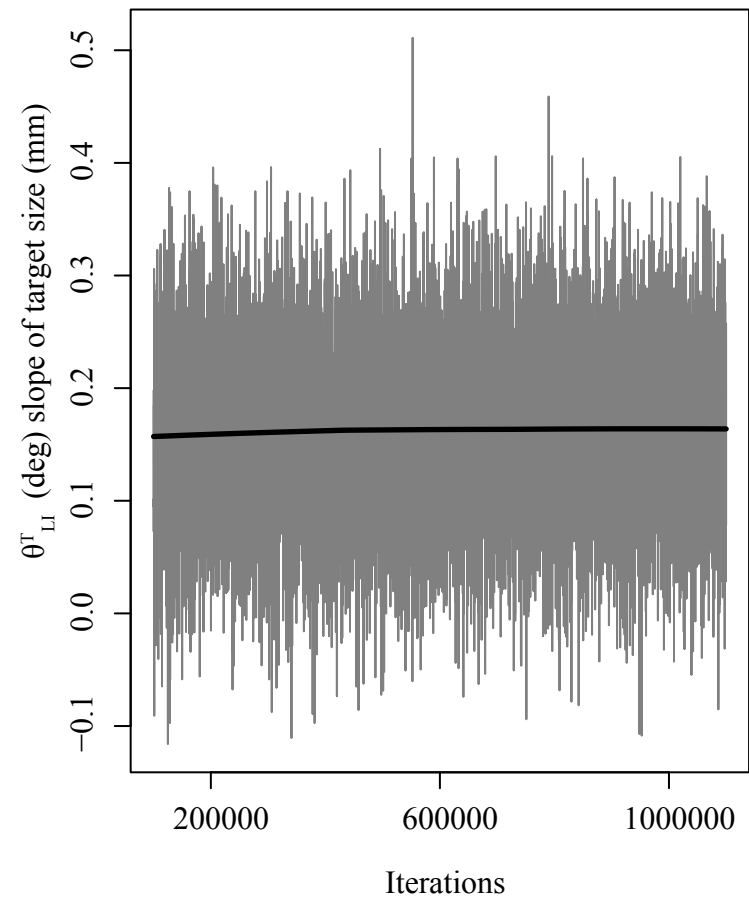
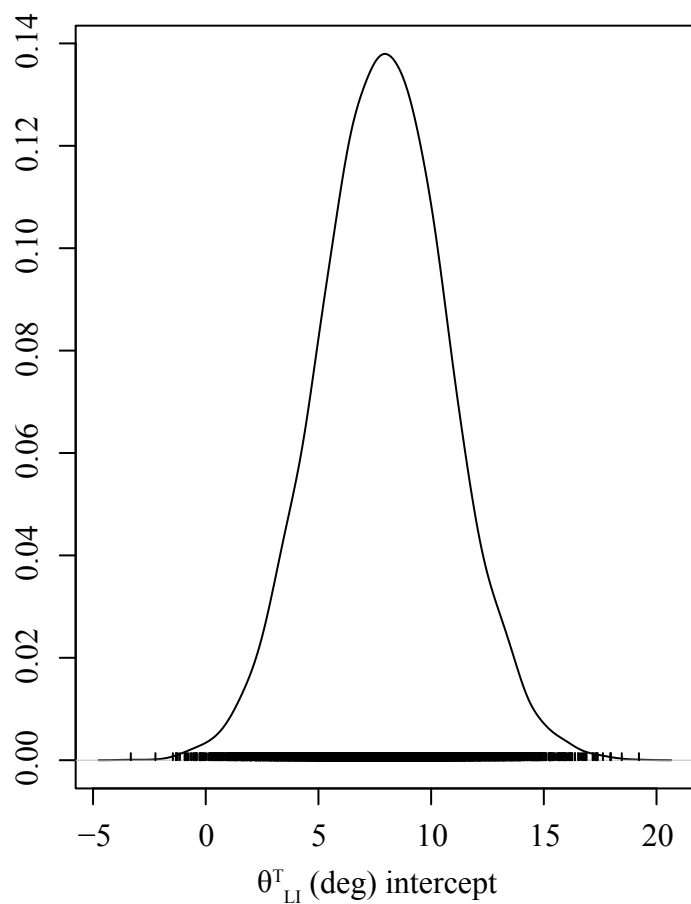
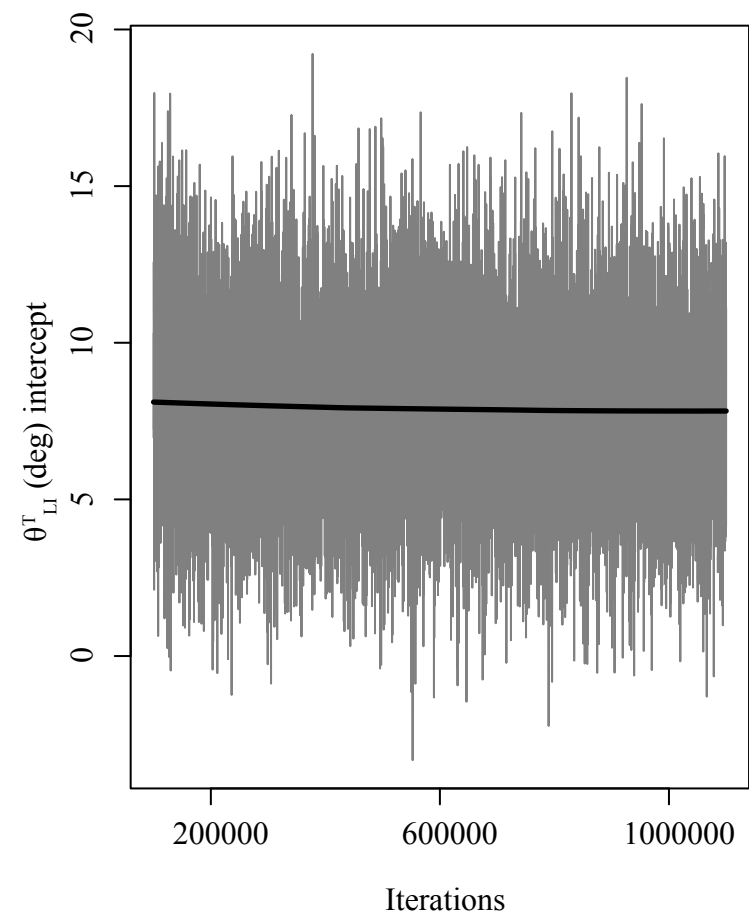
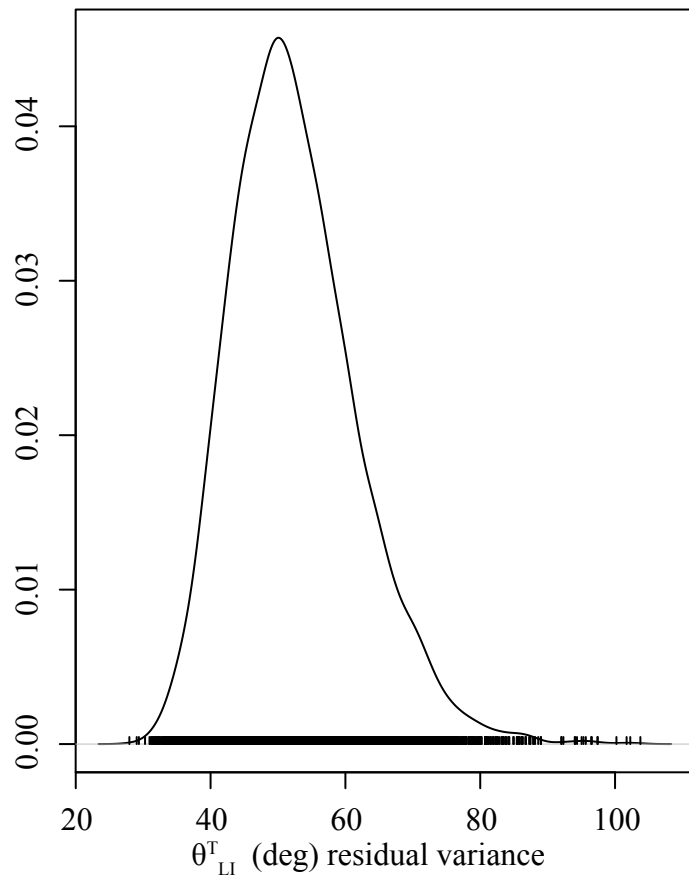
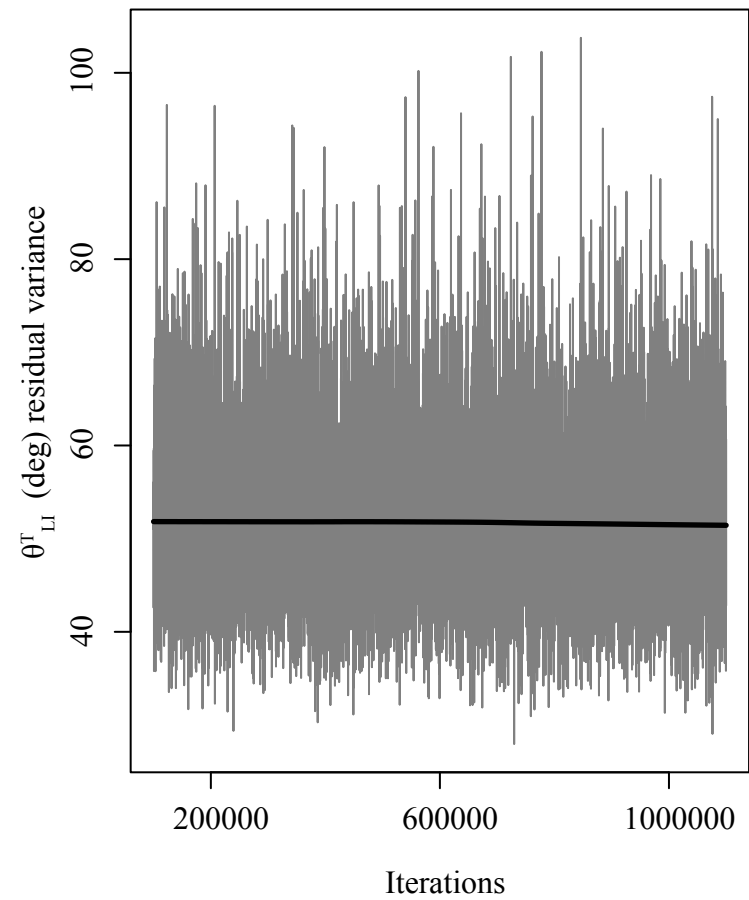
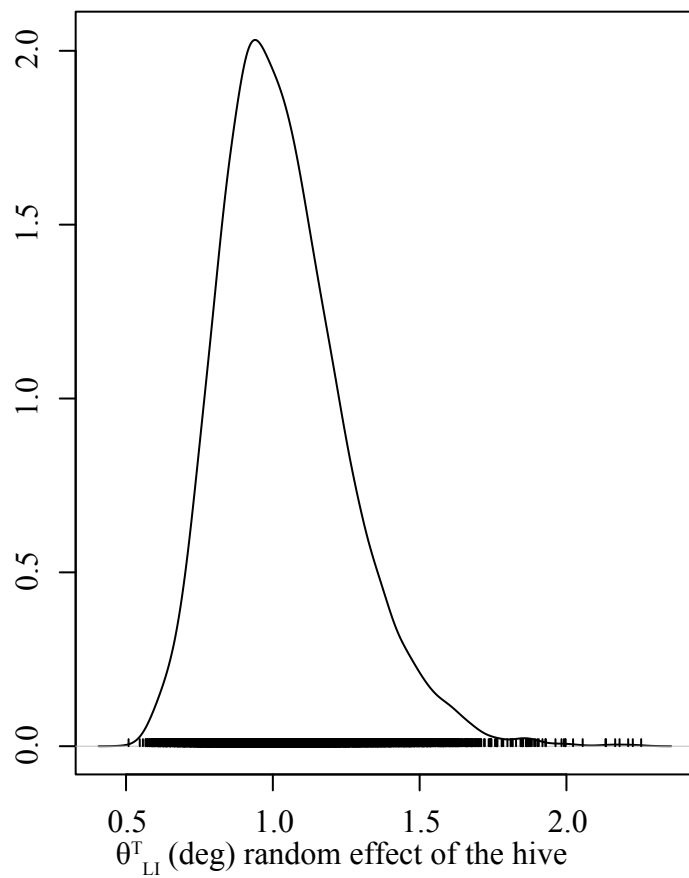
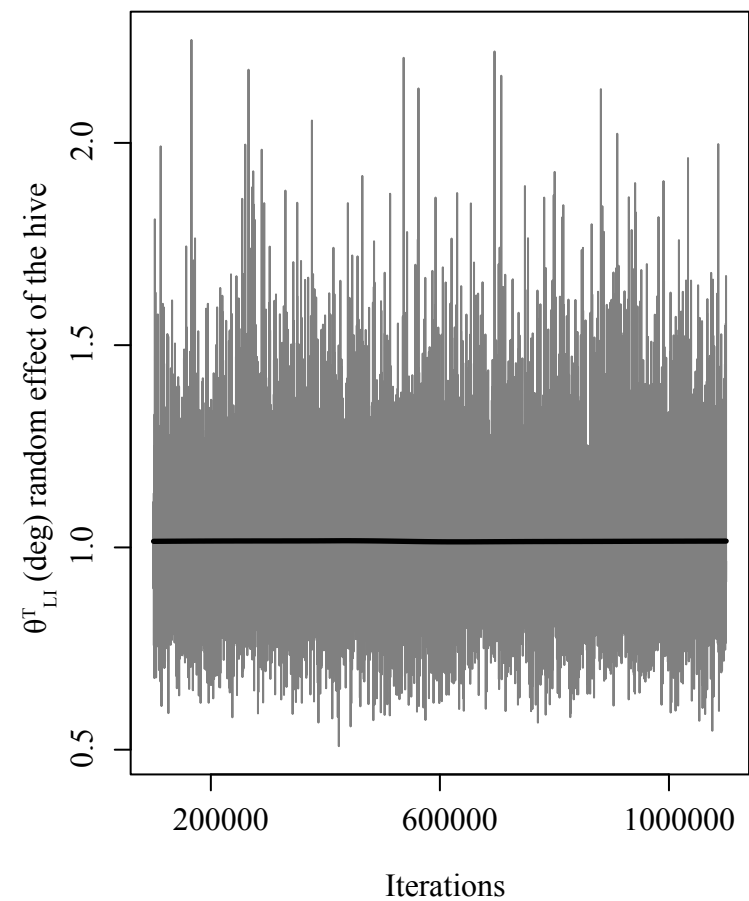
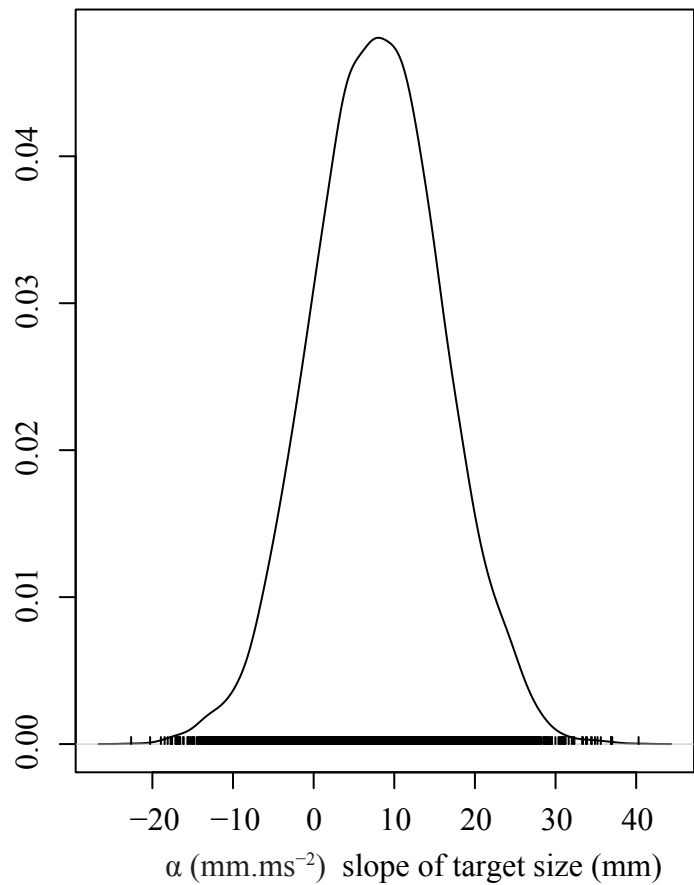
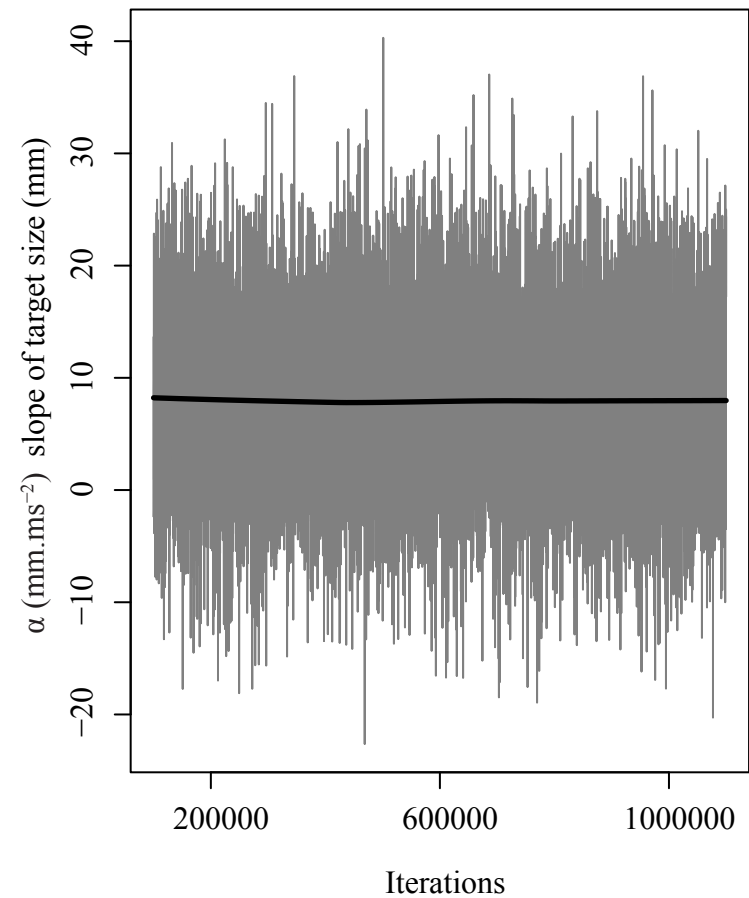
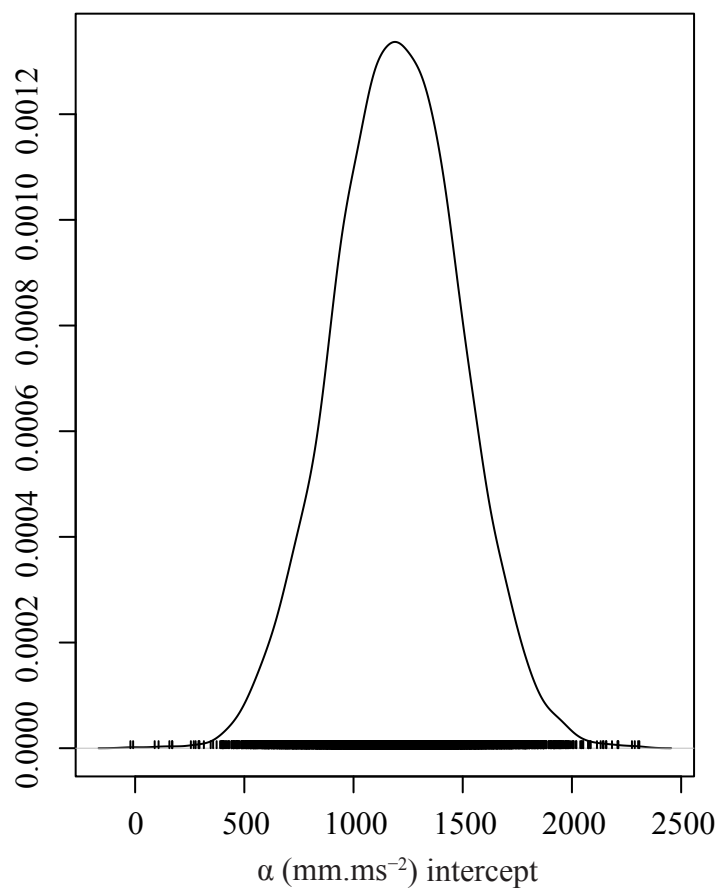
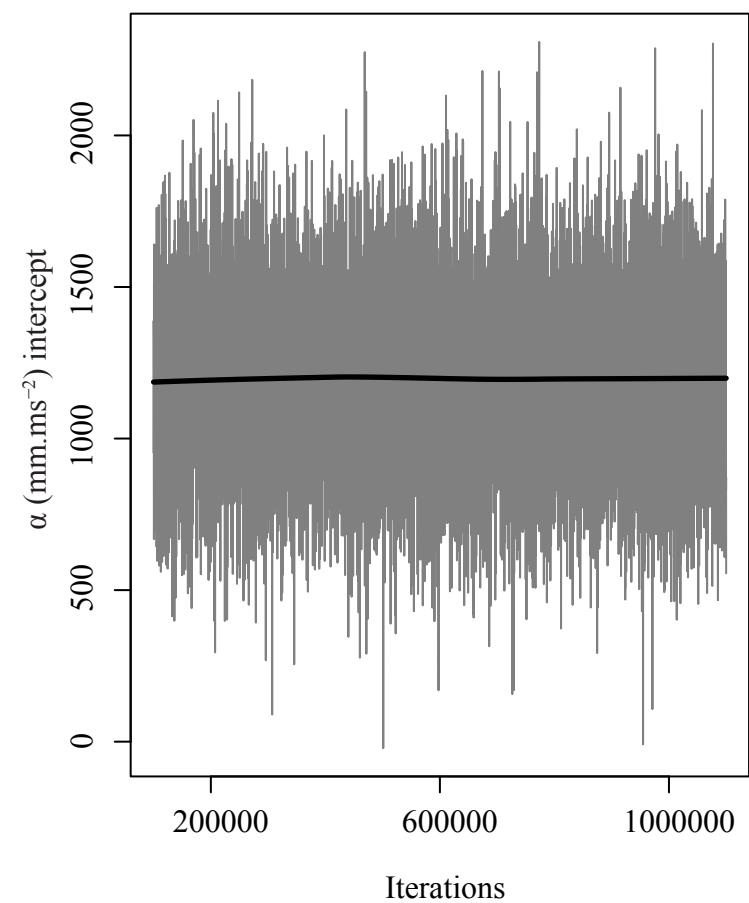


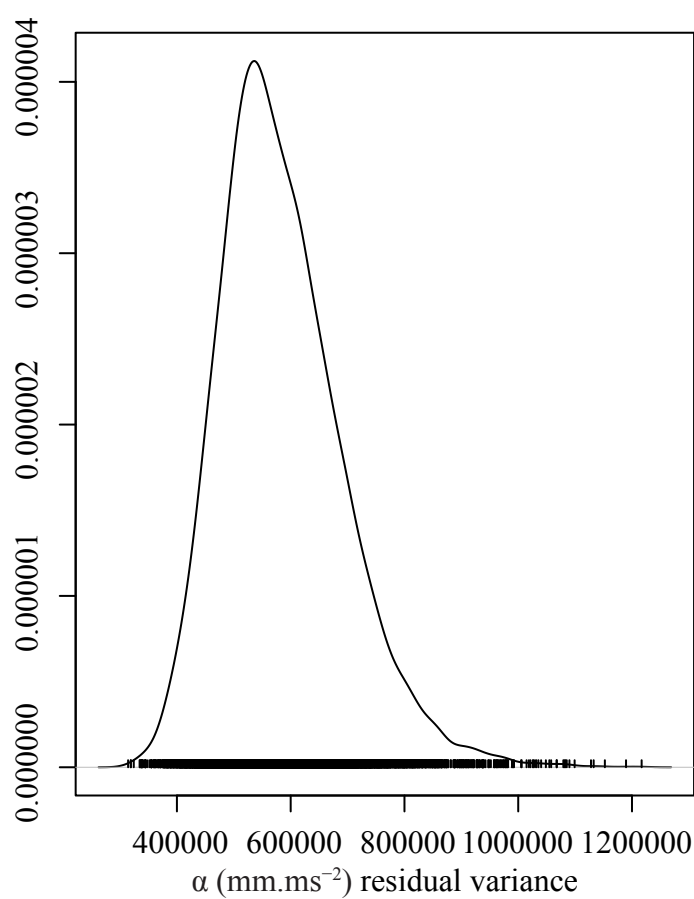
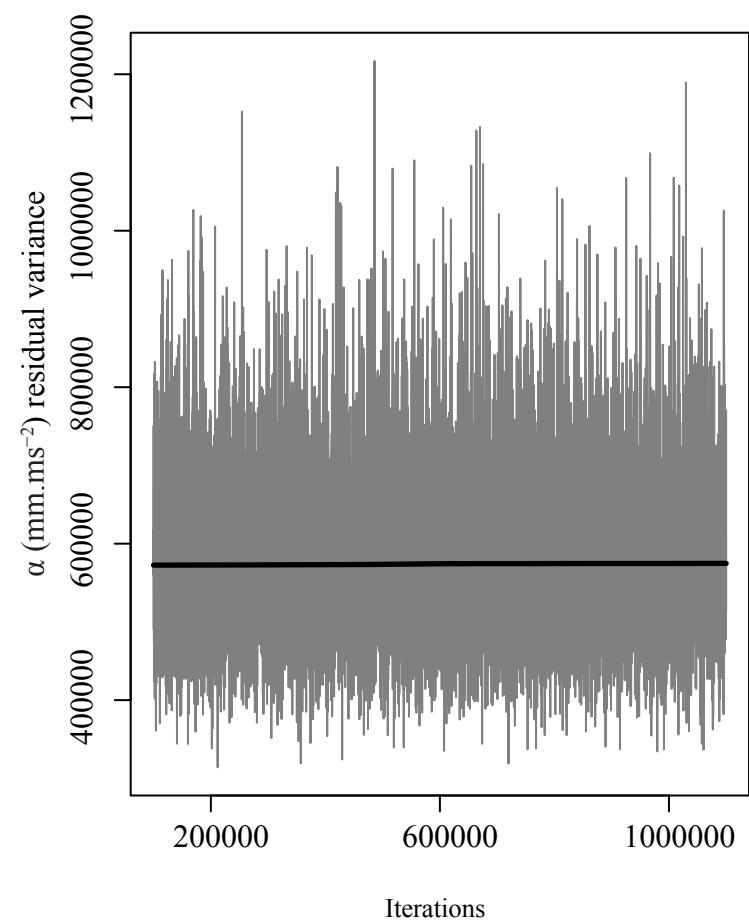
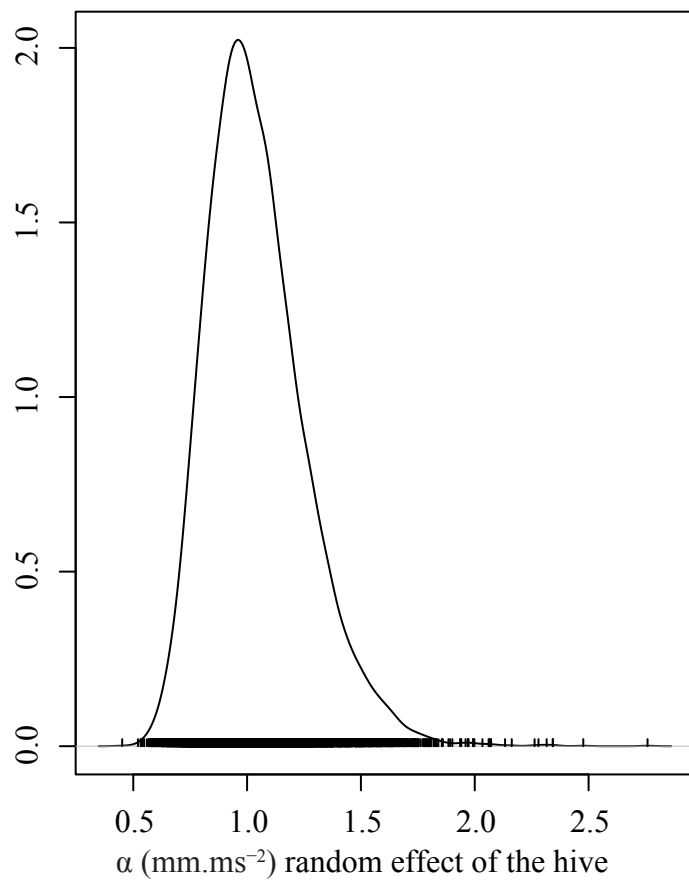
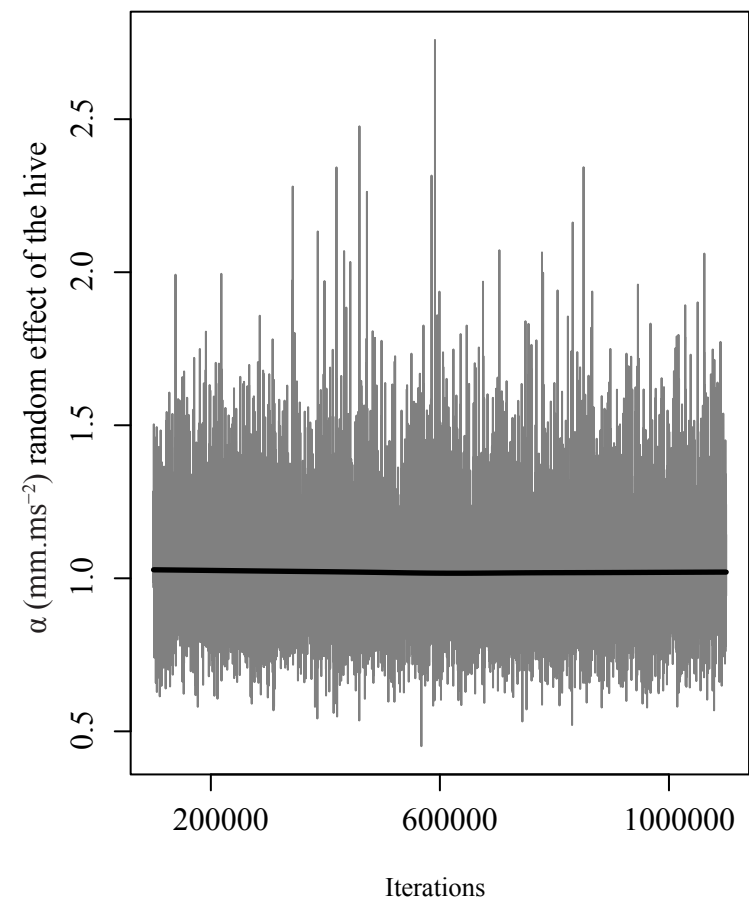
Figure S2:

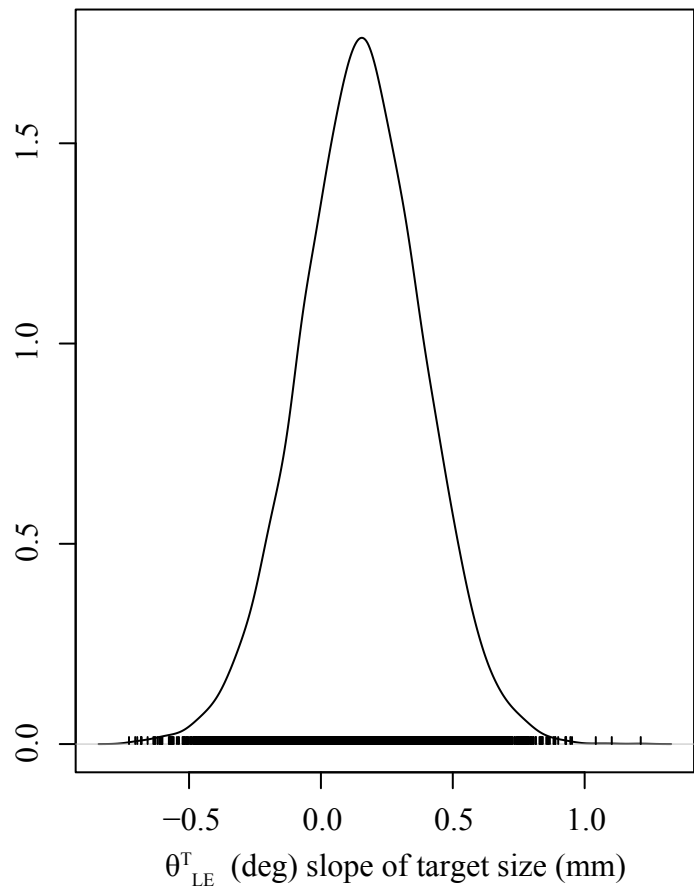
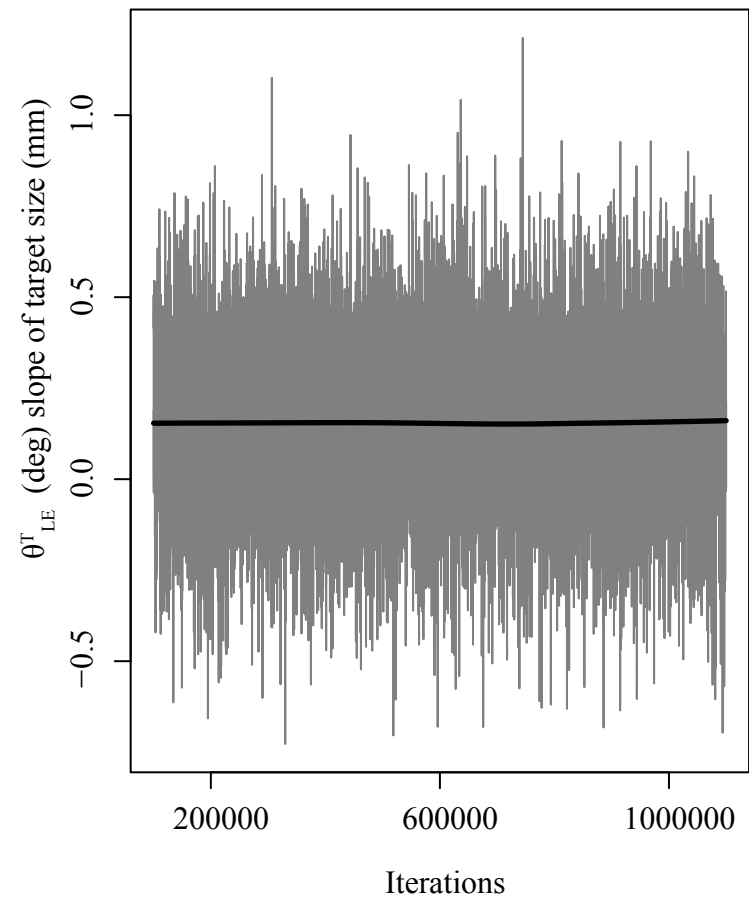
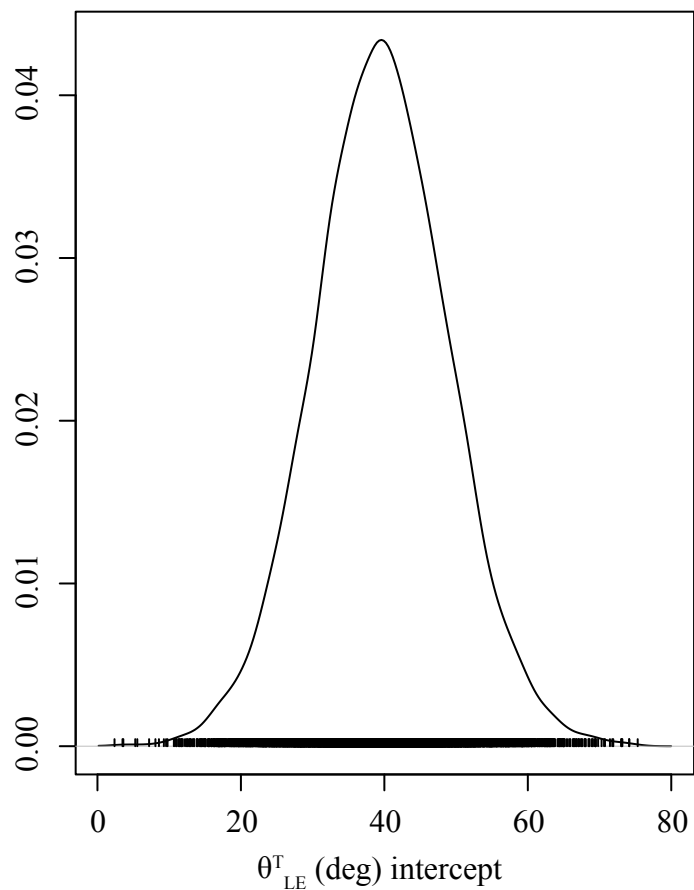
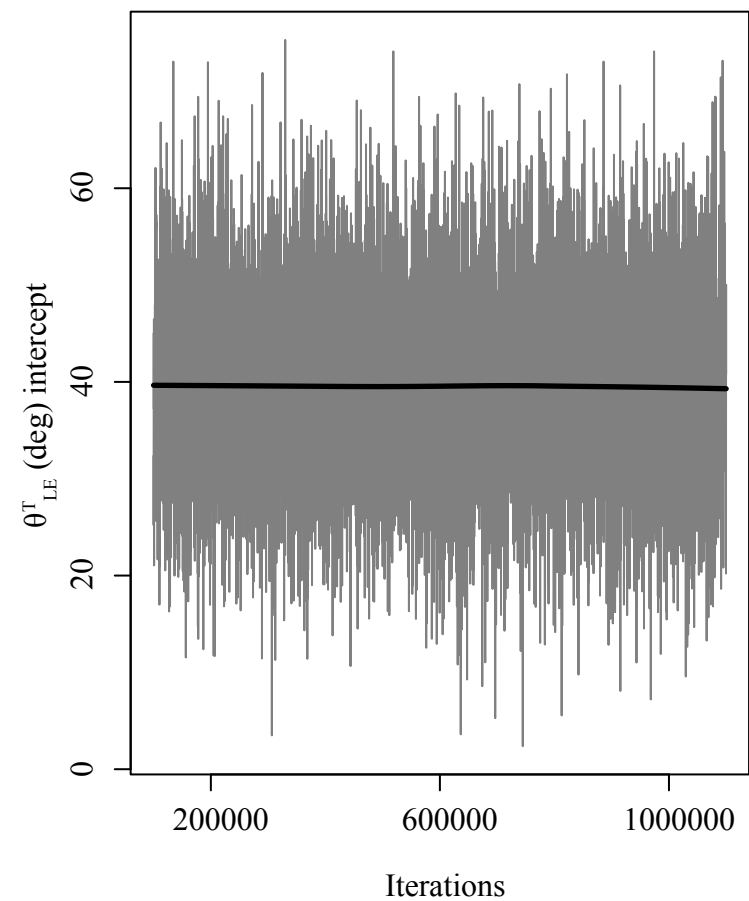
Speed profiles of landing bees in C_{size} as a function of time to contact with different landing types: a final deceleration, ‘type 0’, a deceleration followed by an acceleration, ‘type 1’ or a sustained acceleration, ‘type 2’. The red arrow indicates the change in acceleration, or landing initiation for profiles of type 1-2. Landing were recorded with white sheets surrounding the hive. The speed profiles in $C_{control}$ are available as supplementary material in Tichit et al. 2020.

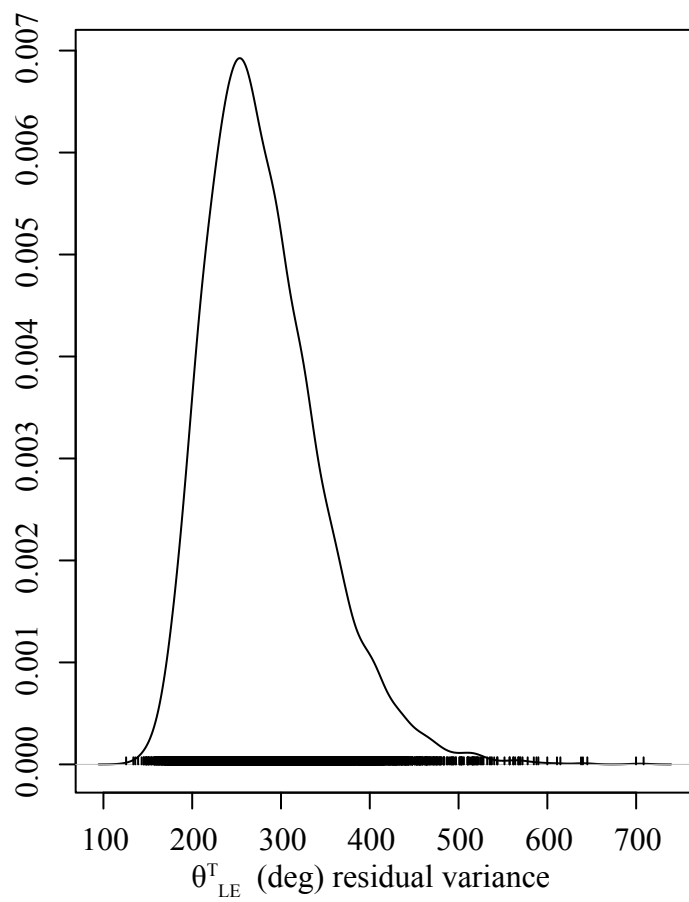
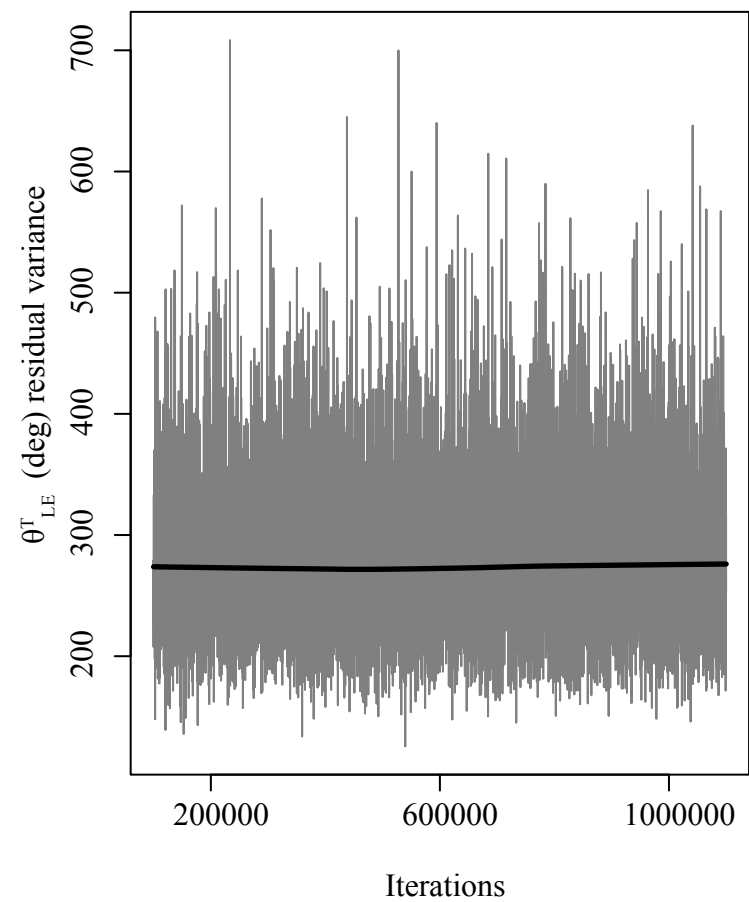
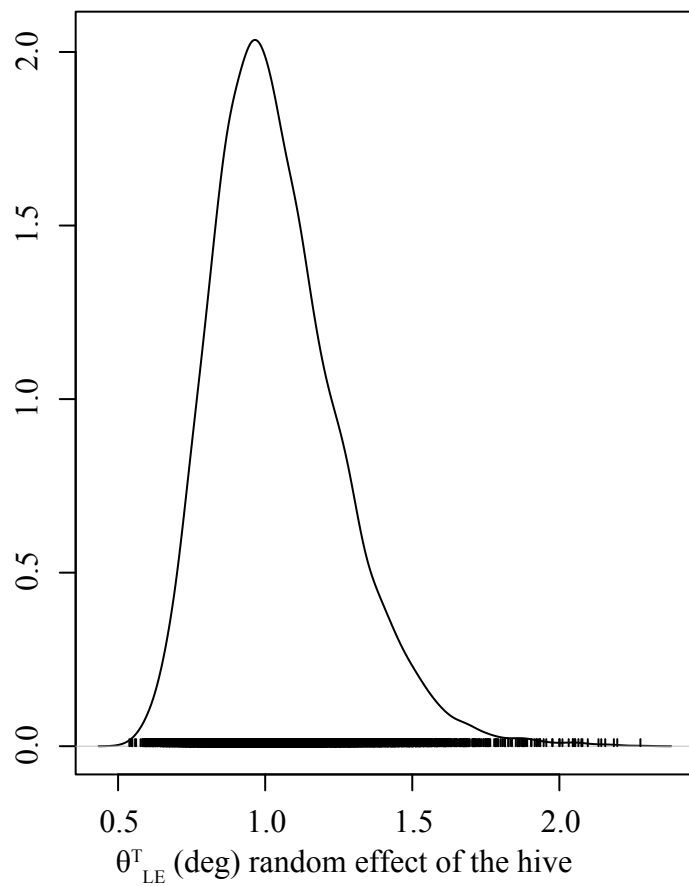
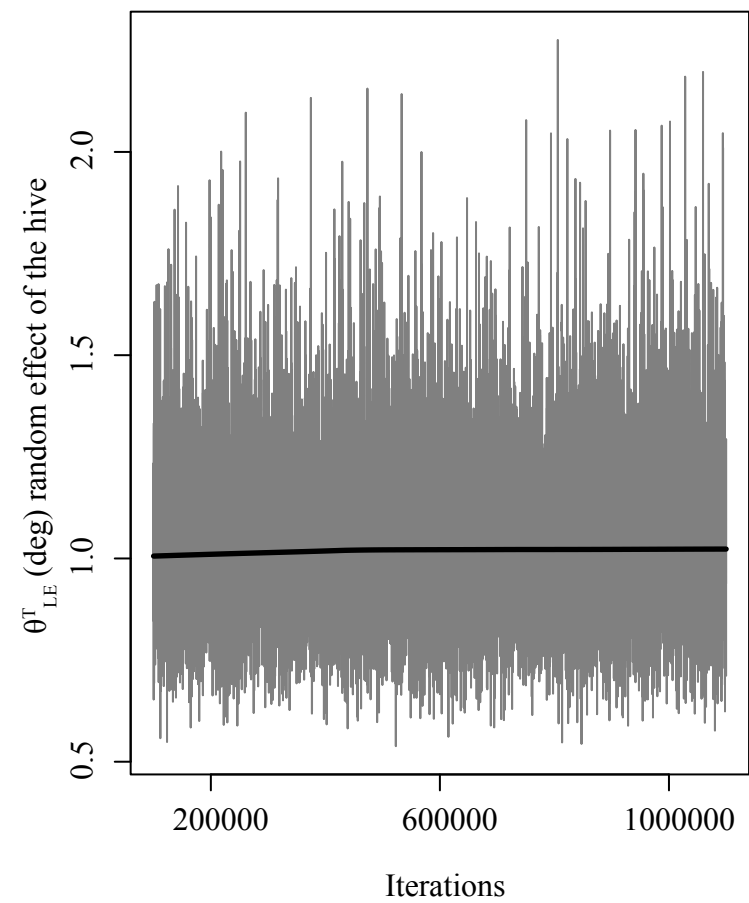


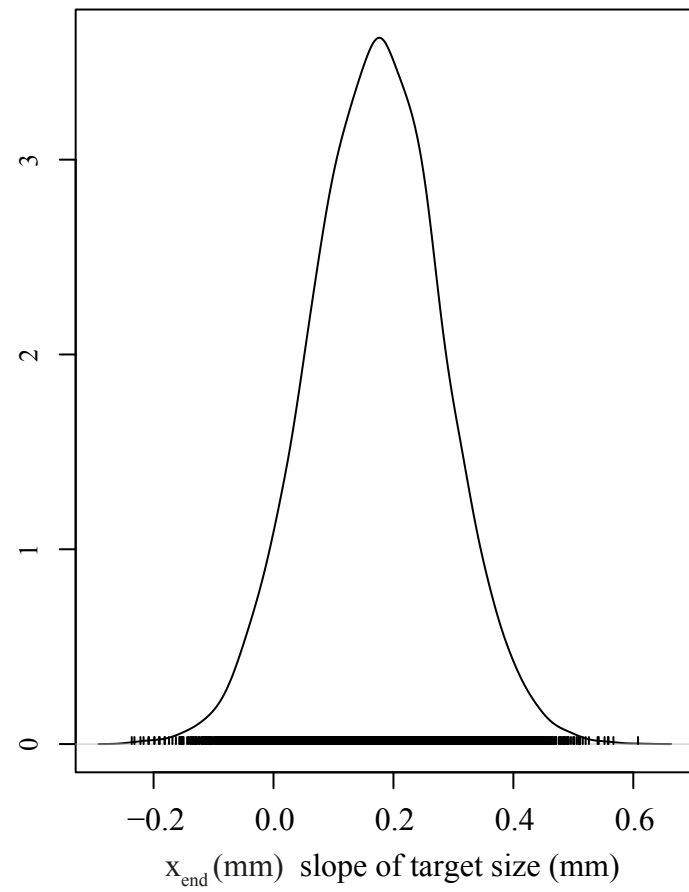
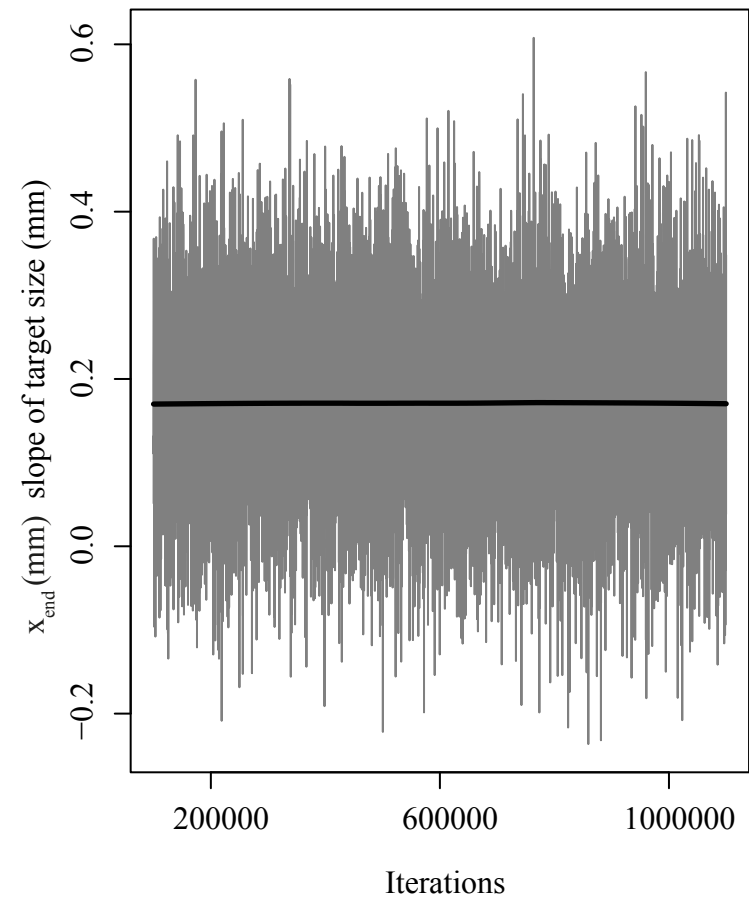
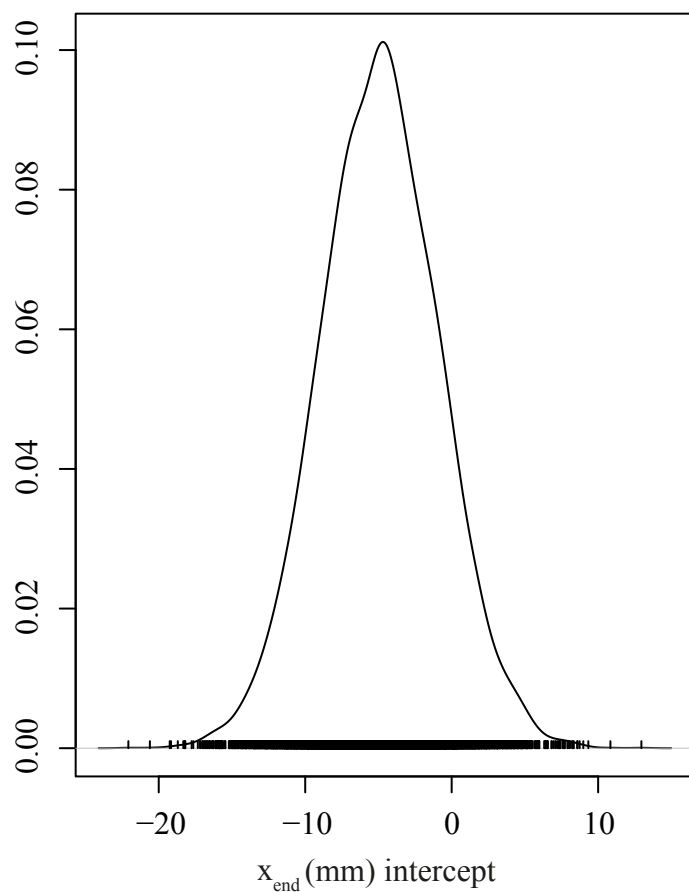
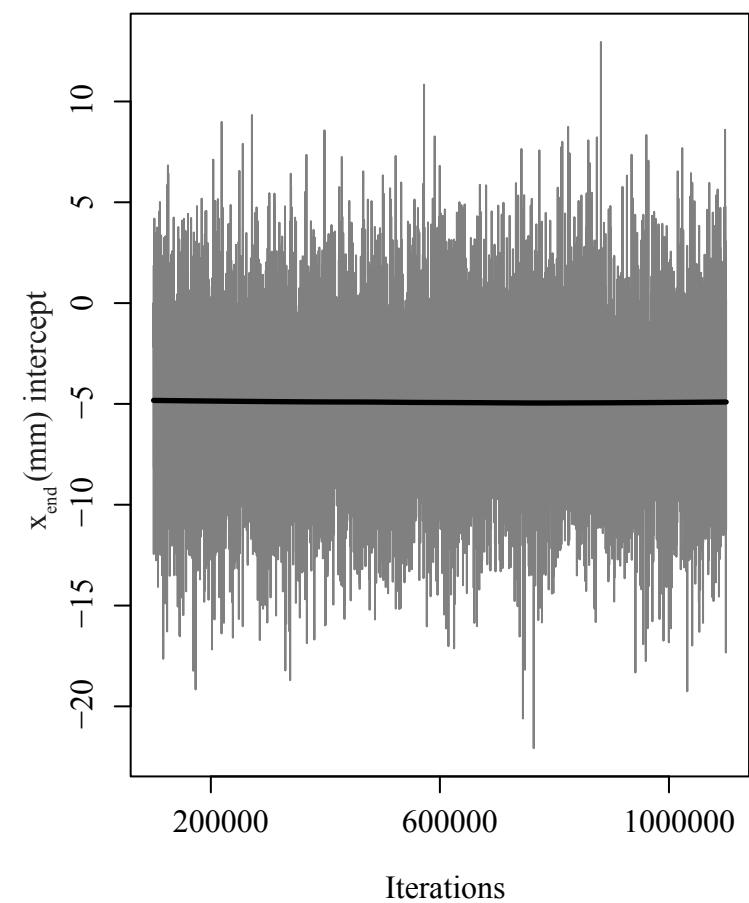


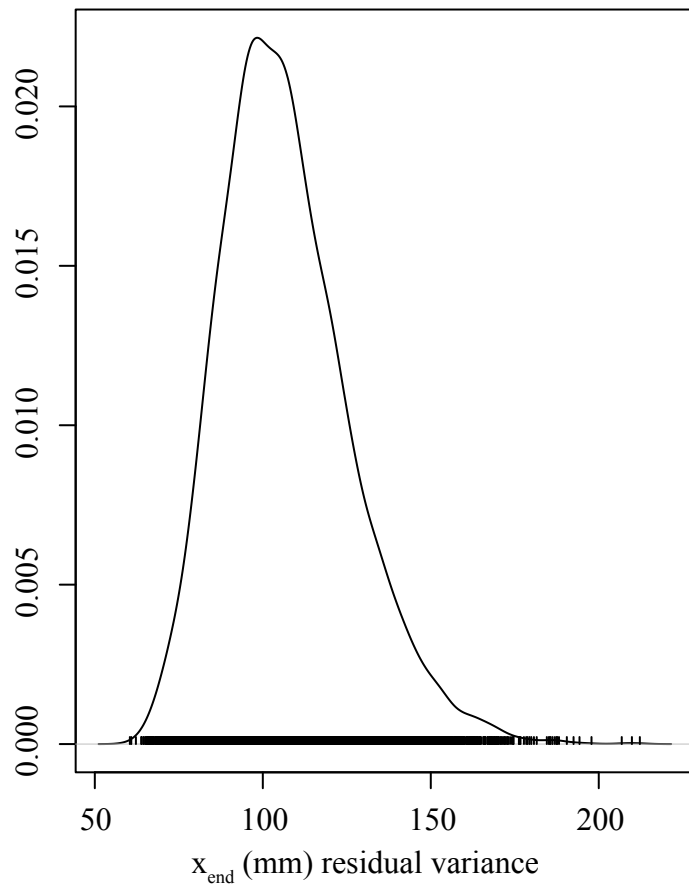
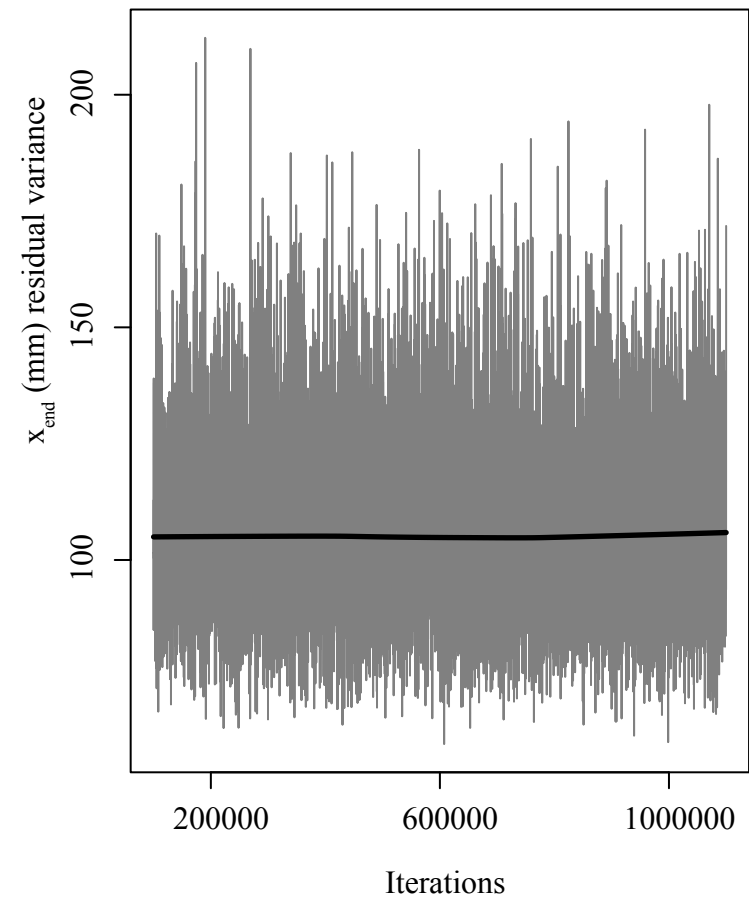
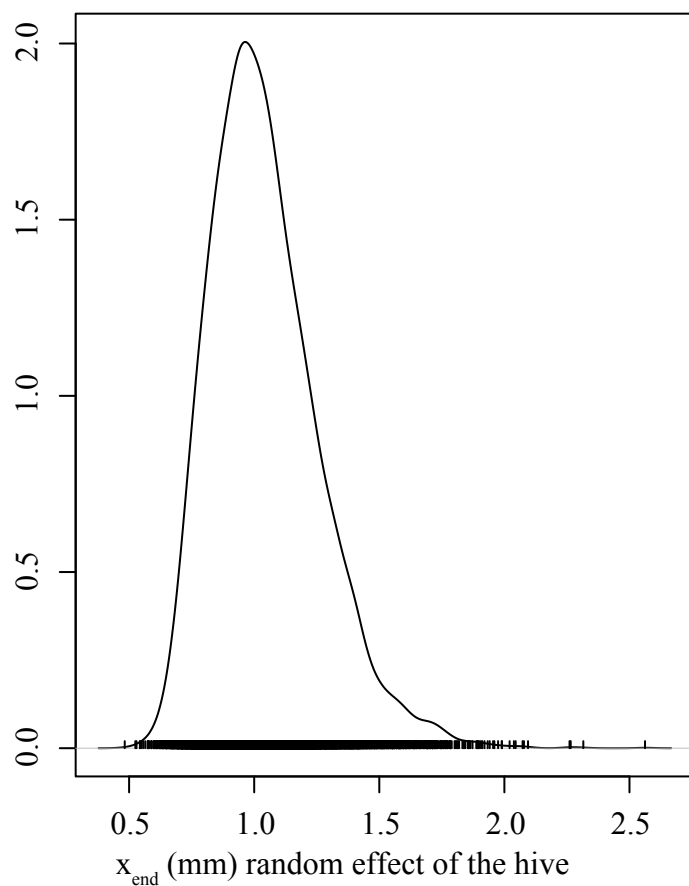
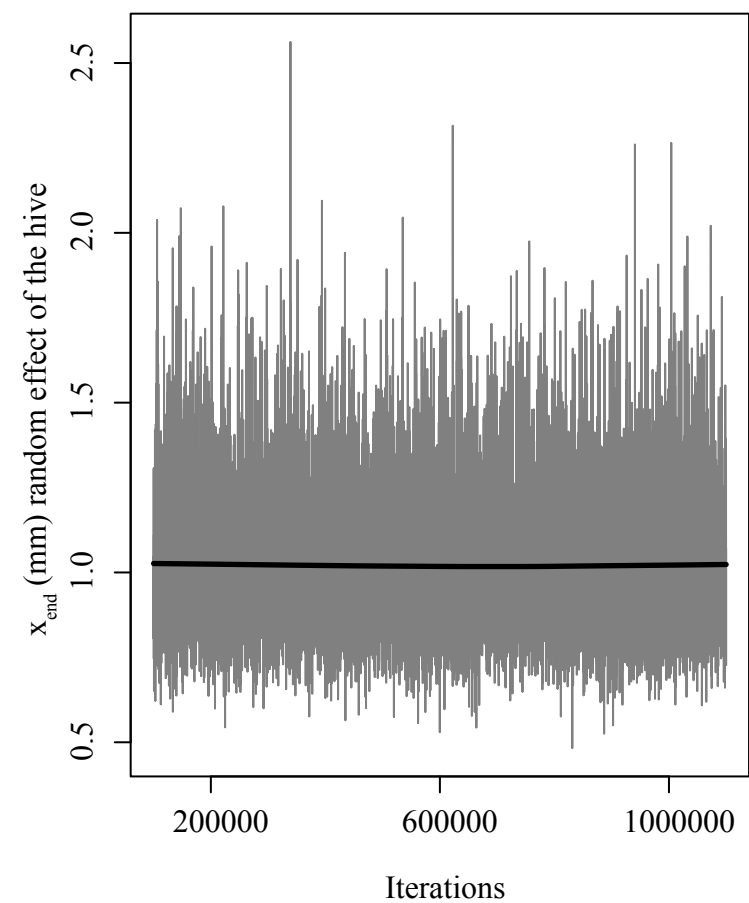


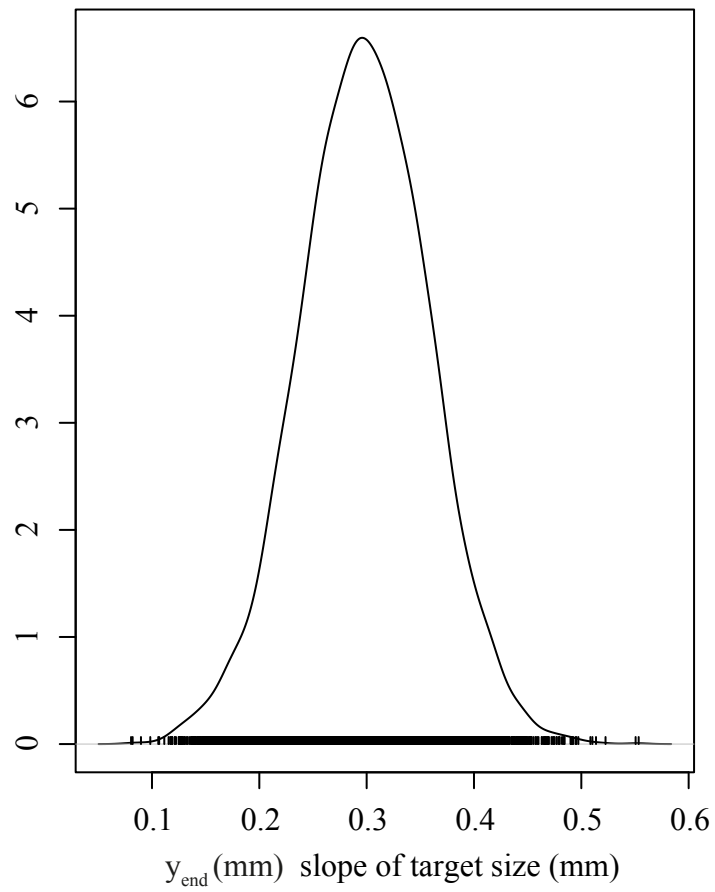
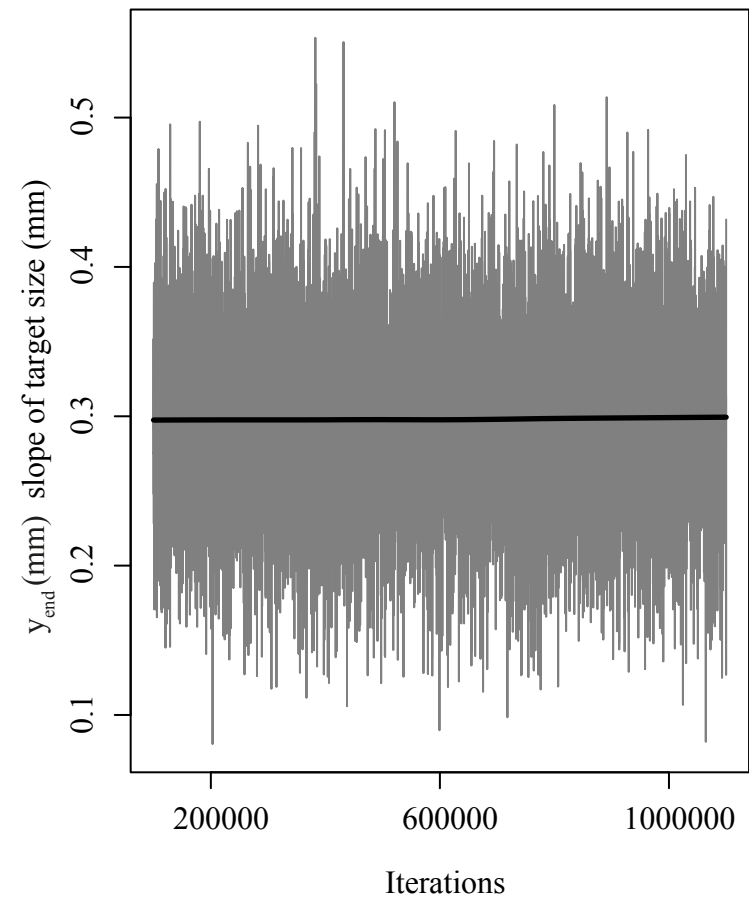
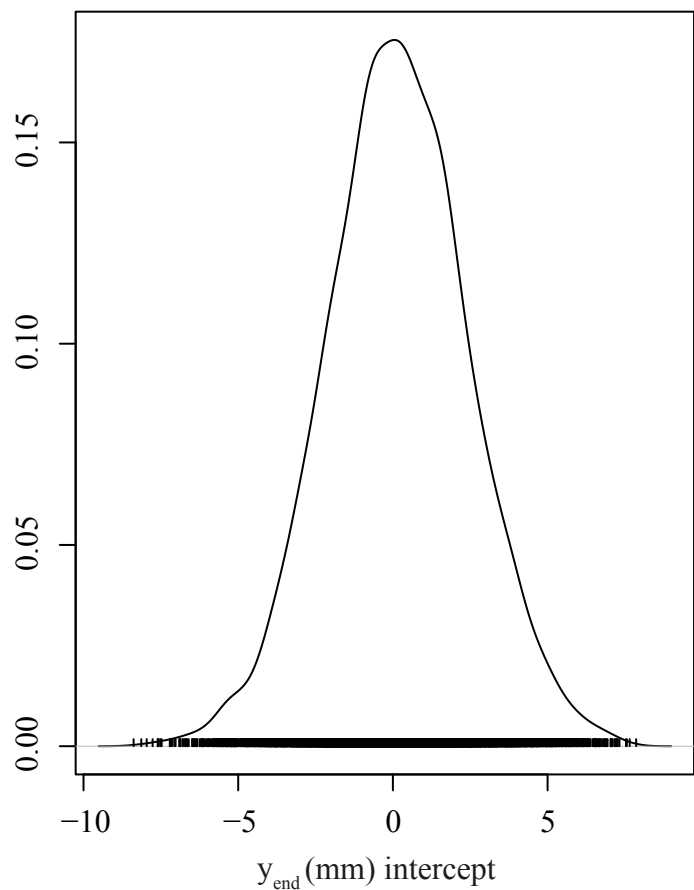
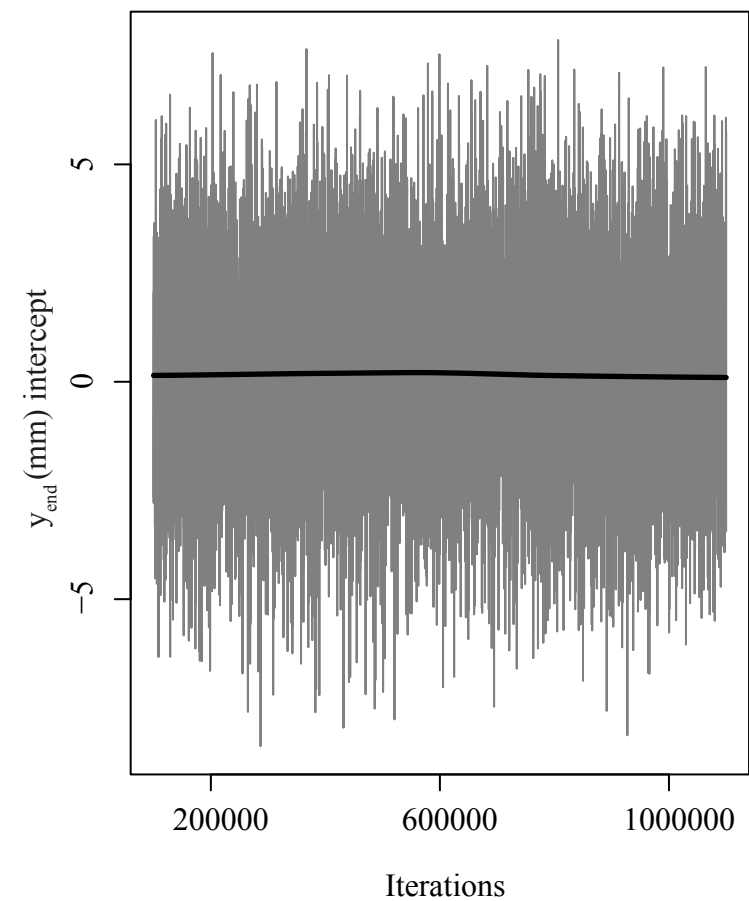












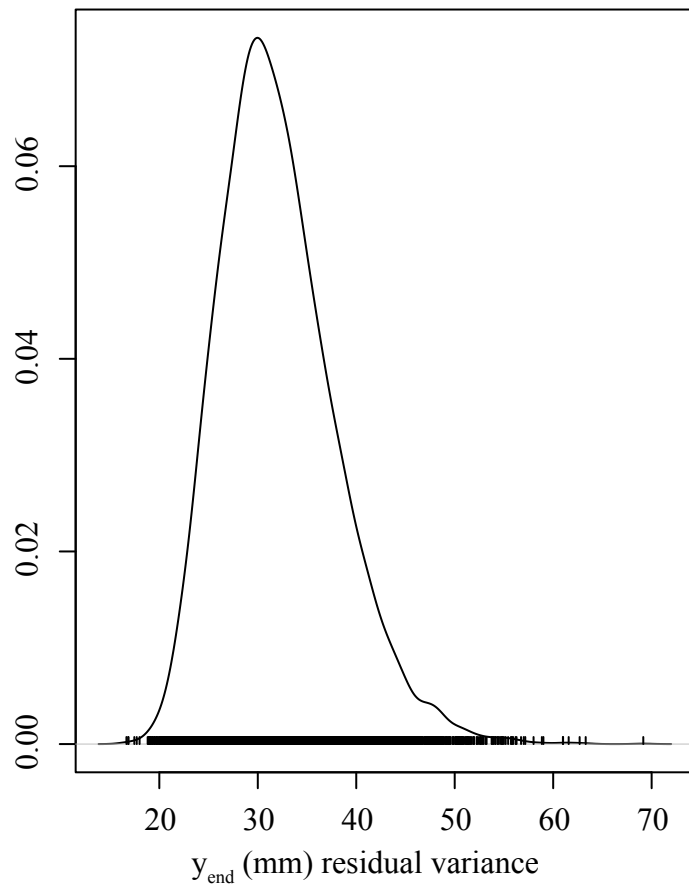
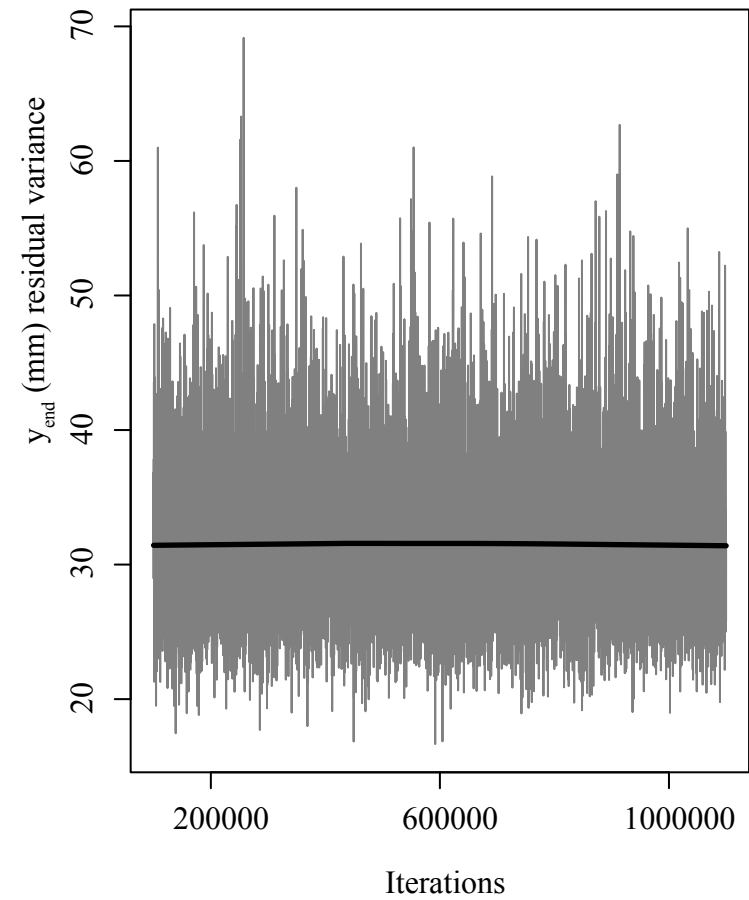
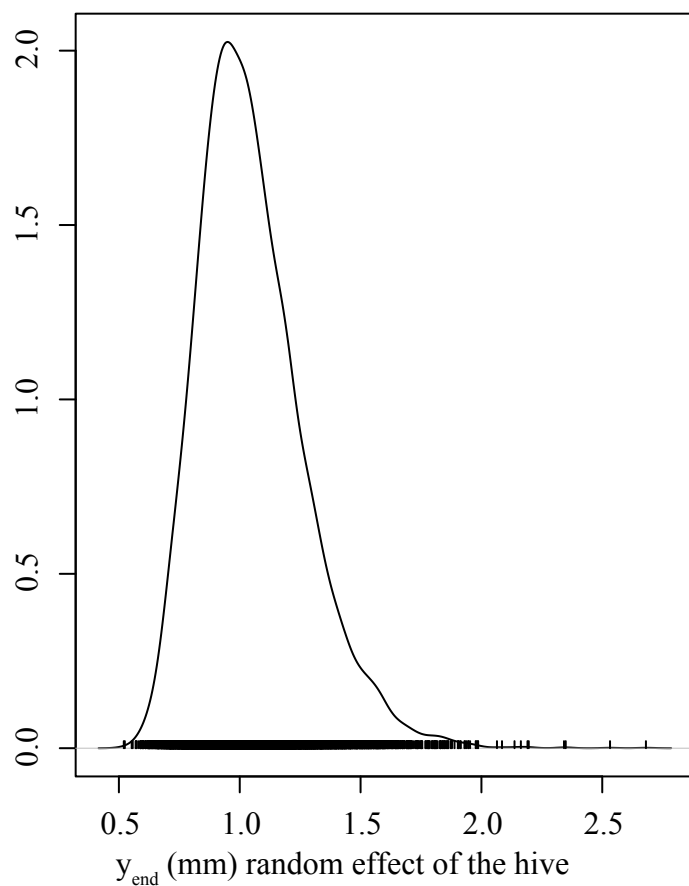
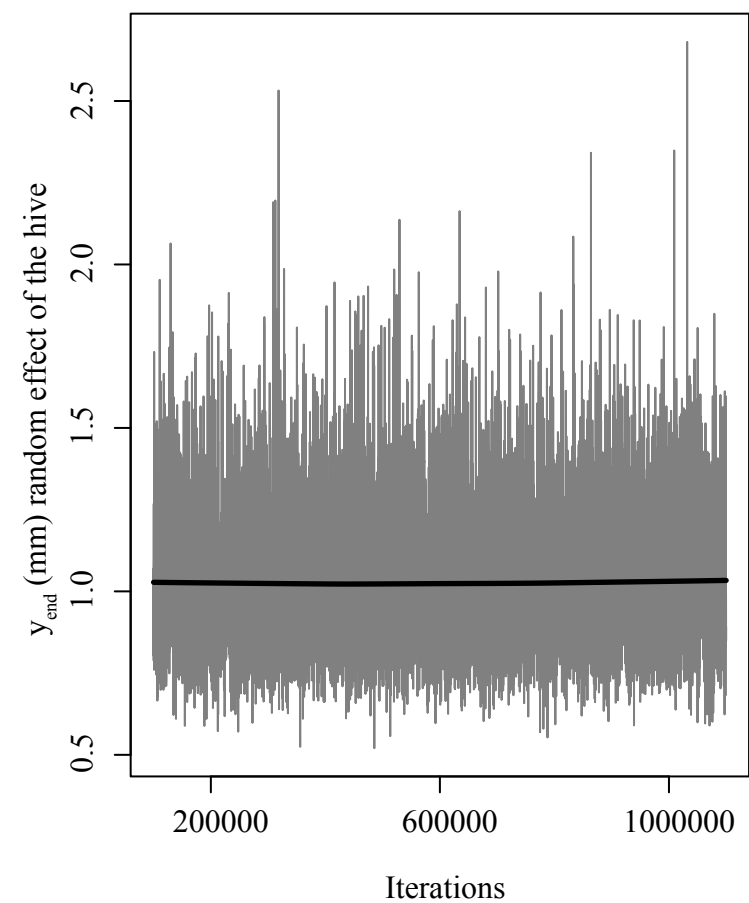


Figure S3:

MCMC traces of the sampled output (left column) and density estimates (right column) of landing parameters for fixed and random effects. Target size (S) was a fixed effect, and hive was a random variable.

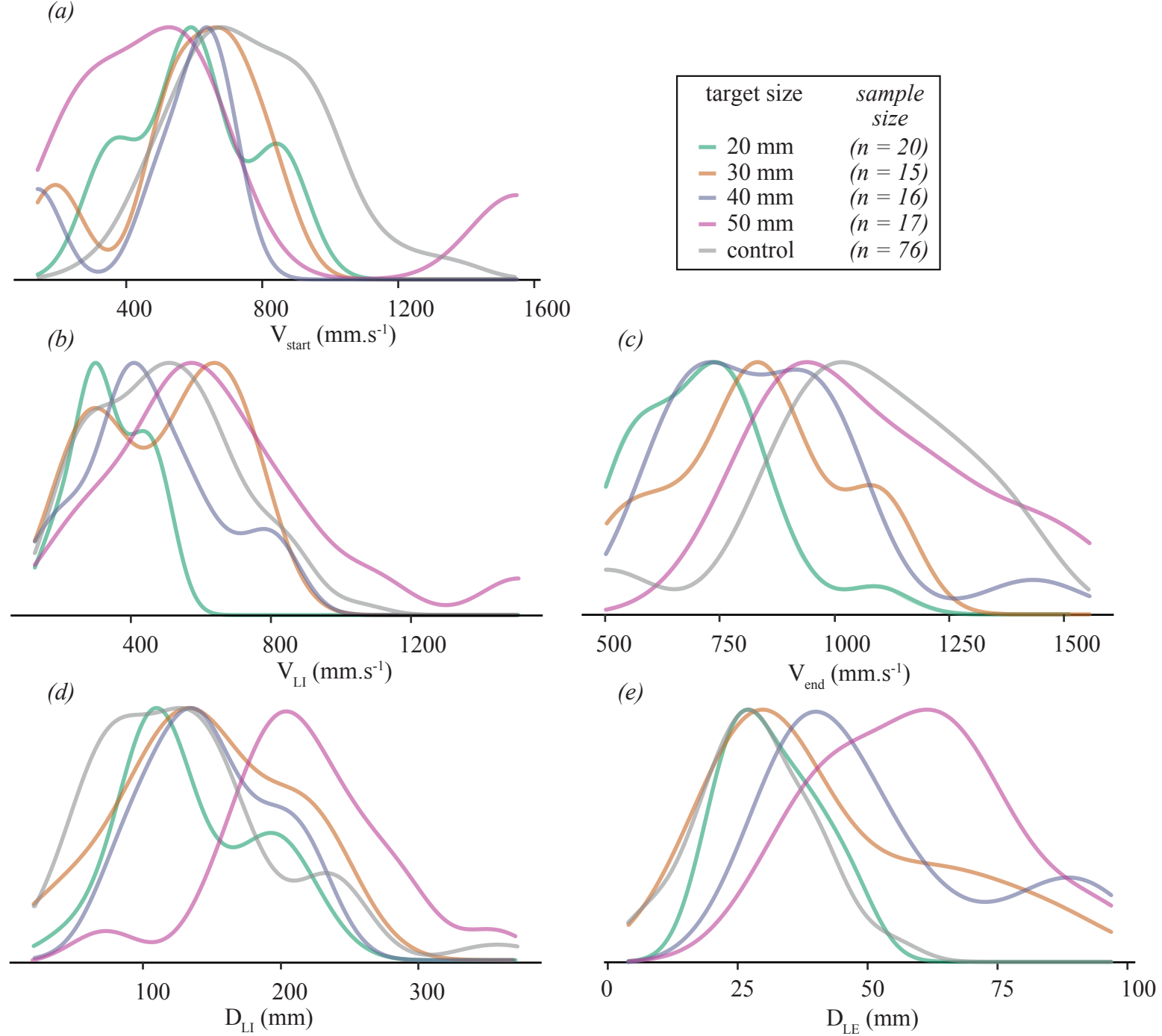


Figure S4:

Normalised densities of the speed at the start V_{start} (a - 250 mm from the target), at landing initiation V_{LI} (b), at the end V_{end} (c), the distance from the hive at landing initiation D_{LI} (d) and the distance from the hive at leg extension V_{LE} (e) separated by target diameter (C_{size}). The profiles for C_{control} are provided for comparison (grey curve).

Smoothing window = 4 frames

<i>parameter</i>	<i>unit</i>	<i>formula</i>	<i>Deviance Information Criterion</i>	<i>Intercept</i>	<i>p_{DICMC}</i>	<i>CI</i>	<i>slope</i>	<i>p_{DICMC}</i>	<i>CI</i>
θ_{LI}^T	deg	1 + S	388	-2.6	ns	[-26;21]	0.72	*	[0.052;1.4]
α	mm.s ⁻²	1 + S	794	-625	ns	[-3609;2281]	107	*	[23;187]
θ_{LE}^T	deg	1 + S	217	30	*	[6.7;54]	0.41	ns	[-0.19;1.0]
x_{end}	mm	1 + S	317	-6.2	ns	[-16;5.1]	0.21	ns	[-0.11;0.50]
y_{end}	mm	1 + S	274	-1.6	ns	[-8.3;5.0]	0.40	***	[0.17;0.53]

Smoothing window = 8 frames

<i>parameter</i>	<i>unit</i>	<i>formula</i>	<i>Deviance Information Criterion</i>	<i>Intercept</i>	<i>p_{DICMC}</i>	<i>CI</i>	<i>slope</i>	<i>p_{DICMC}</i>	<i>CI</i>
θ_{LI}^T	deg	1 + S	399	9.1	**	[3.1;16]	0.15	ns	[-0.023;0.32]
α	mm.s ⁻²	1 + S	984	1254	*	[331;2170]	10.98	ns	[-16;36]
θ_{LE}^T	deg	1 + S	318	36	***	[15;57]	0.26	ns	[-0.27;0.81]
x_{end}	mm	1 + S	413	-3.93	ns	[-11;3.8]	0.10	ns	[-0.10;0.31]
y_{end}	mm	1 + S	355	0.62	ns	[-3.8;5.3]	0.30	***	[0.18;0.42]

Smoothing window = 12 frames

<i>parameter</i>	<i>unit</i>	<i>formula</i>	<i>Deviance Information Criterion</i>	<i>Intercept</i>	<i>p_{DICMC}</i>	<i>CI</i>	<i>slope</i>	<i>p_{DICMC}</i>	<i>CI</i>
θ_{LI}^T	deg	1 + S	448	6.0	***	[2.3;9.5]	0.19	***	[0.10;0.28]
α	mm.s ⁻²	1 + S	1210	1371	***	[852;1892]	3.2	ns	[-11;18]
θ_{LE}^T	deg	1 + S	406	39	***	[23;57]	0.17	ns	[-0.26;0.59]
x_{end}	mm	1 + S	553	-5.8	ns	[-13;1.4]	0.21	*	[0.019;0.40]
y_{end}	mm	1 + S	470	-0.24	ns	[-4.5;3.9]	0.31	***	[0.21;0.43]

Smoothing window = 16 frames

<i>parameter</i>	<i>unit</i>	<i>formula</i>	<i>Deviance Information Criterion</i>	<i>Intercept</i>	<i>p_{DICMC}</i>	<i>CI</i>	<i>slope</i>	<i>p_{DICMC}</i>	<i>CI</i>
θ_{LI}^T	deg	1 + S	476	6.4	***	[2.9;9.9]	0.17	***	[0.084;0.26]
α	mm.s ⁻²	1 + S	1289	1283	***	[756;1782]	4.8	ns	[-9.3;19]
θ_{LE}^T	deg	1 + S	422	38	***	[22;55]	0.20	ns	[-0.22;0.59]
x_{end}	mm	1 + S	589	-5.2	ns	[-12;1.6]	0.19	ns	[-0.0057;0.37]
y_{end}	mm	1 + S	503	-0.64	ns	[-4.9;3.4]	0.31	***	[0.20;0.42]

Smoothing window = 20 frames

<i>parameter</i>	<i>unit</i>	<i>formula</i>	<i>Deviance Information Criterion</i>	<i>Intercept</i>	<i>p_{MCMC}</i>	<i>CI</i>	<i>slope</i>	<i>p_{MCMC}</i>	<i>CI</i>
θ_{LE}^T	deg	1 + S	501	6.6	***	[3.3;9.9]	0.15	***	[0.070;0.24]
α	mm.s ⁻²	1 + S	1362	1180	***	[713;1687]	6.2	ns	[-6.7;20]
θ_{LE}^T	deg	1 + S	453	40	***	[25;56]	0.15	ns	[-0.24;0.53]
x_{end}	mm	1 + S	623	-4.6	ns	[-11;2.2]	0.16	ns	[-0.020;0.34]
y_{end}	mm	1 + S	528	0.42	ns	[-3.8;4.1]	0.28	***	[0.17;0.37]

Tables S3

Linear mixed models of landing parameters in C_{size} with increasing smoothing windows (4 to 20 frames) with target size (S) as a fixed effect and hive as a random variable. The significances of the intercepts and slopes are given by the 95% credible interval (CI) and the bayesian p-value (p_{MCMC}). Significance codes: <10⁻³ ***; <10⁻² **; <0.05 *; >0.05 ns.

<i>type of curve/ Smoothing window</i>	<i>0</i>	<i>1</i>	<i>2</i>
<i>4 frames</i>	73	37	4
<i>8 frames</i>	57	44	14
<i>12 frames</i>	40	51	24
<i>16 frames</i>	35	52	28
<i>20 frames</i>	30	52	33

Table S4

Proportions of landings of type 0 (final deceleration) of type 1 (deceleration followed by acceleration) and 2 (continuous acceleration) in C_{size} with increasing smoothing windows (4 to 20 frames).

<i>Target diameter (mm)</i>	<i>20</i>	<i>30</i>	<i>40</i>	<i>50</i>	<i>control</i>
Landing outside of target/hive (%)	10	13	10	17	7

Table S5

Proportions of landings where touchdown occurred outside of the target disk in C_{control} and C_{size}.

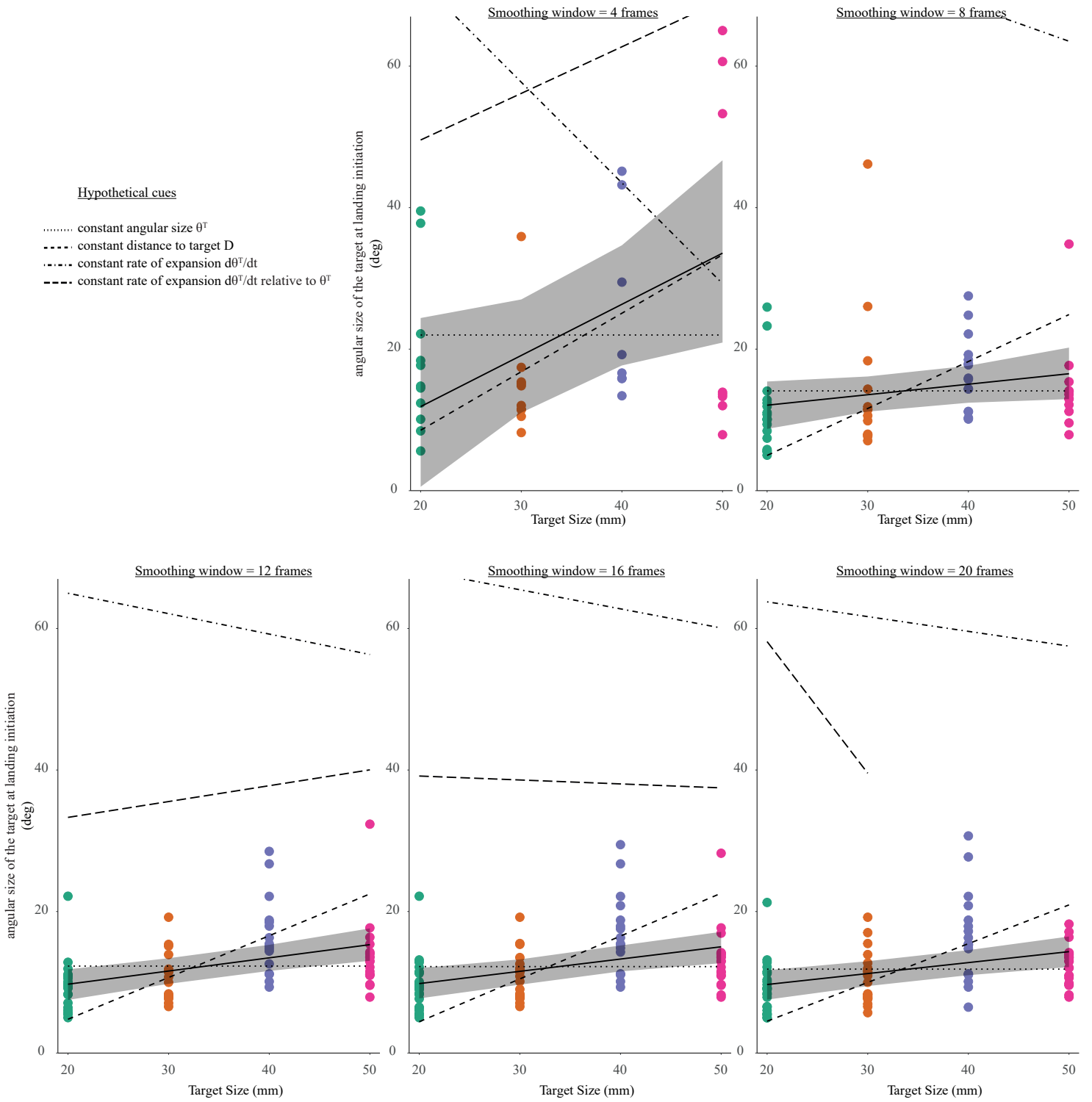


Figure S5

Effect of target size on the angular size of the target with increasing smoothing windows (4 to 20 frames). Solid black lines and grey areas represent a linear mixed model with the 95% credible interval on the observed data (tables S3). Dashed lines represent a linear regression fit on the predicted θ^T if θ^T (medium dashes), D (small dashes), $d\theta^T/dt$ (small and medium dashes), or $d\theta^T/dt$ relative to θ^T (large dashes) would be constant. Note that observed or predicted values of θ^T above 65 degrees are not represented.